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STATUS

PROPOSED SITE PLAN

DRAWING TITLE

121 First Avenue Five Dock, Sydney NSW

PROJECT ADDRESS

Sydney Catholic Schools

CLIENT TITLE

PROJECT TITLE

Domremy College Solais Project

ABN: 84006394261 NSW Nominated Architects:Tom Jordan 7521, Richard Leonard 7522, David Tordoff 8028

Melbourn/

A/135Ground FloorLevel 12,Sturt Street Southbank,11-17 Buckingham Street324 Queen Street,VIC 3006Surry Hills NSW 2010Brisbane Qld 4000T +61 3 9699 3644T +61 2 9660 9329T +61 7 3211 9821

Brisbane

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REV	DESCRIPTION	DATE



LEGEND

- - SITE BOUNDARY EXISTING BUILDINGS



DOMREMY COLLEGE SOLAIS LAB PROJECT STORMWATER MANAGMENT CONCEPT PLAN – CIVIL ENGINEERING





Prepared for: Sydney Catholic Schools By: **en**struct group pty ltd Revision: C February 2018

DOMREMY COLLEGE SOLAIS LAB PROJECT

WATER MANAGEMENT CONCEPT PLAN - CIVIL

ISSUE AUTHORISATION

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<u>u</u> e: <u>sydney@enstruct.com.au</u>

Contents

1	Introduction2	
2	Existing Site Conditions2	
	2.1 Site Description2	
	2.2 Existing Site Drainage2	
	2.3 Site Survey	
3	Project Description	
4	Design Standards4	
5	Stormwater Management and Water Quality4	
	5.1 Drainage Design Criteria and Parameters	
	5.2 Stormwater Collection	
	5.2.1 Roof Levels	
	5.2.2 Surface Water	
	5.3 Water Sensitive Urban Design	
	5.3.1 WSUD Strategy	
	5.3.1.1 Flow Splitter	
	5.3.1.2 Rain Garden5	
	5.3.1.3 Vegetated Swale5	
	5.3.1.4 Pit Inserts5	
	5.3.1.5 Rainwater Tank6	
	5.3.2 Model Setup6	
	5.3.3 Modelling Data & Parameters6	
	ite Description 2 xisting Site Drainage 2 ite Survey 3 act Description 3 gn Standards 4 nwater Management and Water Quality 4 drainage Design Criteria and Parameters 4 tormwater Collection 5 52.1 Roof Levels 5 52.2 Surface Water 5 53.1 VSUD Strategy 5 53.1.1 Flow Splitter 5 53.1.2 Rain Garden 5 53.1.3 Vegetated Swale 5 53.1.4 Pit Inserts 5 53.1.5 Rainwater Tank 6 63.3 Modelling Data & Parameters 6 63.4 Music Model Results 6 6 6 7 7 9 C MODEL 9	
6	On-Site Stormwater Detention	
	6.1 Hydraulic Model7	
7	Sediment and Erosion Control Plan7	
AF	PPENDIX A	
2.0		
AF	PPENDIX B	

DRAINS MODEL	
APPENDIX C	12
CIVIL DRAWINGS	12

1 Introduction

enstruct group have been engaged by Sydney Catholic Schools as civil and structural engineering consultants on the Domremy College Solais Project.

This report:

- Outlines and assesses the condition of existing civil assets on site and provides outline civil engineering guidance to meet the requirements of any future works on the site.
- Establishes the design concept for the civil engineering components of the project including stormwater drainage, Sediment and Erosion Control Plan and Water Sensitive Urban Design.
- Defines the performance requirements for a stormwater management plan, considering the • respective components of the stormwater drainage system, on-site stormwater detention (OSD) and water quality target parameters within the proposed development to suit anticipated and applicable local authority requirements.

Existing Site Conditions 2

2.1 Site Description

The existing site is located in the Domremy College campus at 121 First Avenue in Five Dock, NSW. The site, depicted on Figure 1, is bounded by First Avenue to the north, Ingham Avenue to the east, Fairlight Street to the south and Park Road to the west. Domremy College is situated in a suburban residential area and adjoins Five Dock Park at its northern boundary.

The site is occupied by a number of educational buildings, a carpark and sport facilities. The application site has an approximately area of 28.900 m².



Figure 1: Site Location Plan

2.2 Existing Site Drainage

The site generally falls from a highest point located on First Avenue towards the south-east and south-west corners. Most of the existing development's stormwater runoff is intercepted and diverted to a number of kerb outlets located along Fairlight Street, which fall toward west, and Ingham Avenue

which drains towards Fairlight Street. There is not exists stormwater network surrounded the site, therefore the public drainage is limited to street drainage.

Survey plans only show pits and grated drains with their respective invert levels; however, the existing internal stormwater pipe network information was not indicated on plans.

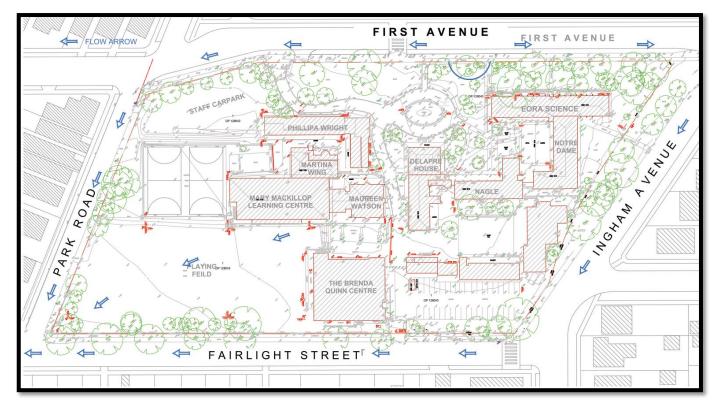


Figure 2. Existing Drainage

2.3 Site Survey

An overall survey of the existing site was undertaken by:

Surveyor Name:	LTS Lockley
Surveyor Contact Details:	Suite 1, Level 1 810 Pacific Highway, Gordon NSW 2072 Tel: 1300 587 000
Job Reference:	43724DT
Survey Date:	September 2016
Drawing Number:	13 Sheets

Project Description 3

The proposed development include the

- Demolition of a car park •
- Demolition of the Orleans and Darby Centre buildings ٠
- Construction of a new library and year 7 & 8 learning hub, to be located on south-east corner of the site
- Construction of a new staff car park on the north-west corner as shown in Figure 3.

The proposed development application site is about 5990 m², of which 4700 m² for the 2-storey Solais Project and surrounded area, and the rest to the car park.

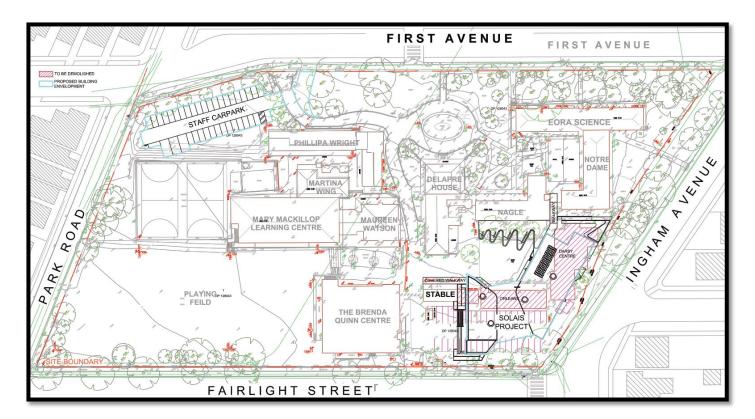


Figure 3: Building Location Map (figure to be updated with latest layout)

Design Standards 4

The following list indicates the relevant design guidelines and standards to be considered during the design of the project:

- Australian Rainfall & Runoff: Volume 1 & 2
- AS3500.3 Plumbing and Drainage: Stormwater Drainage •
- Drainage Model Drawings RTA. ٠
- Guide to Road Design, Part 5 Drainage Design AUSTROADS (2008).
- AS 3500.3-1990 National Plumbing and Drainage Code Stormwater drainage.
- Waterway Design (A Guide to the Hydraulic Design of Bridges, Culverts and Floodways) -• AUSTROADS 1994.
- Managing Urban Stormwater: Soils and Construction, "The Blue Book" 4th edition 2004. •
- Concrete Pipe Selection and Installation Concrete Pipe Association 1990. ٠
- Canada City Bay Council Development Control Plan 2017 •
- MWRC Development Design Specification D5 Stormwater Drainage Design •

Stormwater Management and Water Quality 5

The overall site stormwater management objectives applicable to the site were identified as follows:

- Provision of safe overland flow paths within development an on public land.
- Provision of controls such as on-site stormwater detention, community basins and the like and onsite retention systems to reduce and control stormwater runoff.
- The installation of pipe/channel systems to minimise hazard to pedestrian and vehicular traffic caused by uncontrolled surface stormwater runoff.
- The installation of water quality control devices such as trash screens, gross pollutants traps, water quality ponds and the like and encouraging the use of water sensitive urban design to protect the quality of receiving waters.

According to Council's guidelines and the type of development, the following control types would be applied:

- On-site Stormwater Detention System (OSD)
- Water Sensitive Urban Design (WSUD)

The Stormwater Management Strategy proposed for site development has been prepared with consideration of the above objectives and Council's requirements and guidelines. The strategy focuses on minimising the impacts of the development on the adjoining properties and maximising the environmental, social and economic benefits achievable by utilising responsible and sustainable stormwater management practices.

5.1 Drainage Design Criteria and Parameters

The key design criteria and council requirements for stormwater drainage design are as follows:

- · Post-Development stormwater discharge peak for event up to 100 year ARI storm is not to exceed the Permissible Site Discharge (PSD) calculated through the Catchment Based Method.
- Underground stormwater drainage system to be design to capturing the runoff produced from a 20 ARI storm.
- Concentrated discharge is limited to 25 l/s per 15 lineal metre of frontage for all storm event;
- Stormwater to drain by gravity to Council's stormwater system;

Drainage has been designed in accordance with the methods outlined in "Australian Rainfall and Runoff", Institution of Engineers. The software package DRAINS was used to design the new stormwater network including the OSD.

5.2 Stormwater Collection

5.2.1 Roof Levels

Gutters and downpipes will be designed by the Hydraulic Engineer. The roof drainage system of gutters, downpipes and associated pipework is to be designed in accordance with AS/NZS 3500.3 Plumbing and Drainage Part 3: Stormwater Drainage.

Downpipes conveying rainwater from the roof level of the proposed building will be connected to rain water harvesting tank or high early discharge chamber in OSD tank.

5.2.2 Surface Water

Runoff from the area adjacent to the new building, will be captured and conveyed by proposed stormwater pits and pipes to OSD tank.

Due to the topography, a small green area of the proposed development will be by passing the proposed detention system to discharge to council kerb and gutter.

5.3 Water Sensitive Urban Design

The development will achieve the pollution reduction targets identified in City of Canada Bay DCP by utilising water sensitive urban design (WSUD) treatment initiatives. The pollutant reduction requirements outlined in Table 1 below have been adopted as the minimum values for water quality treatment.

Table 1 Pollutants reduction target.

Pollutant Type	Percentage Retention of Post-development Loads
Total suspended solids (TSS)	80%
Total phosphorus (TP)	45%
Total Nitrogen (TN)	45%
Gross Litter	All Litter - 70% Material (>50mm) - 70%

5.3.1 WSUD Strategy

The WSUD Strategy proposed for the development may utilises a treatment train approach, consisting of the following: flow splitter, rain gardens, catch pit inserts and vegetated swales.

5.3.1.1 Flow Splitter

Flow splitters are specially designed to protect water quality devices, located downstream of the unit, of high flows produced by infrequent storms. The main objective of this device is split the low (up to 1 in 3 months ARI) from the high flow in the system.

A flow splitter is proposed downstream of the OSD tank. Low flow will be directed to a vegetated swale, whereas high flow will be diverted to the existing stormwater network to be discharged in council kerb and gutter.

5.3.1.2 Rain Garden

Raingardens are specially designed garden beds which filter stormwater runoff from surrounding areas or stormwater pipes. They are also called bio-retention systems as they provide biological treatment of stormwater using soil, plants, roots and microbes.

A raingarden lets water collect and settle on the garden surface then soak through the plants and filter media. Sediment is trapped on the surface. Nutrients dissolved in the stormwater are used by the plants and toxins stick to the soil. The soil and plant roots work together to naturally filter the water and remove pollutants.

A 20 m² raingarden has been proposed next to the new Staff Carpark.

5.3.1.3 Vegetated Swale

Vegetated swales are typically trapezoidal or dish-shaped open channels provided to convey and filter stormwater runoff through vegetation to remove coarse sediment and total suspended solids. Overflow pits will be provided within the swale to take in excess flows and discharge them into drainage system.

Vegetated swales are proposed along the south-west boundary to convey surface water to proposed OSD tank, as well as on the south-east corner on Fairlight Street as final link of the proposed treatment train.

5.3.1.4 Pit Inserts

Pit inserts, also known as litter baskets, are considered as an at-source primary treatment solution. It is an efficient and cost-effective pre-screening primary treatment system that captures and retains gross pollutants at drainage entry points. Pit inserts, consisting of a capture basket and a filter mesh liner, are usually fitted below the road invert or surface of the pit and hence are visually unobtrusive.

Pit inserts can be customised to fit almost any stormwater inlet pit and the mesh liner opening could vary depending on the targeted capture of solids, sediment and attached pollutants. Cleaning of the pit inserts is undertaken either manually or using a small vacuum truck. The cleaning frequency MUSIC Modelling.

5.3.1.5 Rainwater Tank

In addition to water savings, the rainwater harvesting tank will help reduce runoff volume from the proposed development during small storms and associated stormwater pollutants that would discharge from the site.

The Rainwater tank have not been defined at this stage, therefore is not shown in the model. However, the benefit of its use will be reflected as an extra improvement to the proposed treatment system.

5.3.2 Model Setup

A detailed water quality analysis to be develop using WSUD strategy for the proposed development to meet Council's water quality targets. The water quality modelling for this study will be undertaken using the industry standard software model MUSIC (Model for Urban Stormwater Improvement Conceptualisation) Version 6.2.

5.3.3 Modelling Data & Parameters

The nearest rainfall station with a reasonable period of 6-minute rainfall data is Sydney (Station 066037) which is about 14 km from the site. In MUSIC, rainfall data is available for this station from 1/01/1990 to 21/12/1999. However, for water quality modelling purposes, only rainfall data for the 6-minute period was used. Apart from addressing the required data length of 10 years, this period was selected for the guality and continuity of the available rainfall data. The mean annual rainfall (MAR) during this 10-year period is 1,035 mm which is slightly lower than the long-term MAR of 1,261 mm which was calculated from the rainfall data sourced from the Bureau of Meteorology (BOM) website.

The soil / groundwater parameters and the pollutant loading rates adopted for the site for Total Suspended Solids (TSS), Total Phosphorus (TP) and Total Nitrogen (TN) used in the MUSIC model are consistent with the values recommended by both Sydney Metropolitan Catchment Management Authority (SMCMA) and Sydney Catchment Authority (SCA) guidelines.

5.3.4 Music Model Results

The MUSIC model generated for the development was used to estimate the annual pollutant loads attributed to the pre and post-development as well as the resultant pollutant loads leaving the site after flows go through the proposed treatment train.

The results show that the estimated average annual pollutant export loads from the proposed development have been reduced using the adopted treatment train stormwater management measures and that the treatment targets set at neutral or beneficial effect (NorBE) and Council's DCP guidelines have been met. The proposed treatment train is outlined in APPENDIX A.

	Sources	Residual Load	% Reduction
Flow (ML/yr)	6.15	6.07	1.3
Total Suspended Solids (kg/yr)	1140	90.1	92.1
Total Phosphorus (kg/yr)	2.28	0.638	72
Total Nitrogen (kg/yr)	15.4	8.31	45.9
Gross Pollutants (kg/yr)	143	0	100

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Table 2. Music Model Results

6 On-Site Stormwater Detention

On-site stormwater detention (OSD) is required by Council to ensure there is no increase over the PSD in discharges from the site resulting from storm events up to the 100-year ARI event. This requirement applies to all developments that discharge stormwater into Council's drainage system and where an overland escape route or overflow system is provided for storms in exceedance of the 100-year ARI event.

Council's Catchment Based Method has been applied adopting the application area (5990 m²) as site area, to determinate the Site Storage Requirement (SSR) and Permissible Site Discharge (PSD):

- SSR (200 m³/hectare) = 120 m³
- PSD (180 L/s/hectare) = 108 L/s

Due to the natural topography of the site and the restrictions mentioned in 5.1, two separates systems has been designed to restrict the flow in both the new car park as well as in the proposed new building.

A sag pit system has been proposed to reduce the discharge rate from the carpark. This system controls the flow by restricting the inlet capacity of the pit, providing storage on-grade.

The remaining catchment of the developed site area will be attenuated in an OSD system which will be designed as a below ground detention tank.

The proposed system has managed to reduce the discharge under the PSD values all ARI storm events up to the 100-year ARI as follow:

- 33 l/s carpark peak discharge
- 51 l/s OSD peak discharge
- 17 l/s by-pass area peak discharge

6.1 Hydraulic Model

A DRAINS hydraulic modelling has been undertaken to analyse and design the stormwater drainage network. The components of the system have been divided in two smaller models for practical reasons. The results of both models have been included in Appendix B for council verification.

Pit location and pipes invert levels and sizes, well as all the components of the system are detailed on the Civil Drawings (refer Appendix C). A long section to demonstrate that OSD will not have drowned outlet, has also been included in mentioned Appendix.

7 Sediment and Erosion Control Plan

The erosion and sediment control measures adopted for the development during the construction phase have been designed in accordance with Council guidelines and Soils and Construction – Managing Urban Stormwater – Landcom.

Erosion and sediment controls will be provided during the construction phase in accordance with Council guidelines. These control measures have been developed alongside consideration of the necessary earthworks associated with the development.

A sedimentation and erosion control plan has been prepared for the site works, and is provided in Appendix B. The plan includes measures such as: sediment fences surrounding disturbed areas to capture sediment runoff and a truck shaker tray at each point of access to the work area. The measures to be adopted are summarised in the Table 2.

Final details of sediment and erosion control measures for the early works and main works will be implemented on site by the successful contractor who will be provided with these drawings. The contractor will take into account the site works staging including the preferred site access points, site shed locations and temporary stockpile locations in developing and implementing these requirements but will be ultimately responsible for managing temporary stormwater and sediment and erosion control during construction.

Table 3. Sedimentation control measures

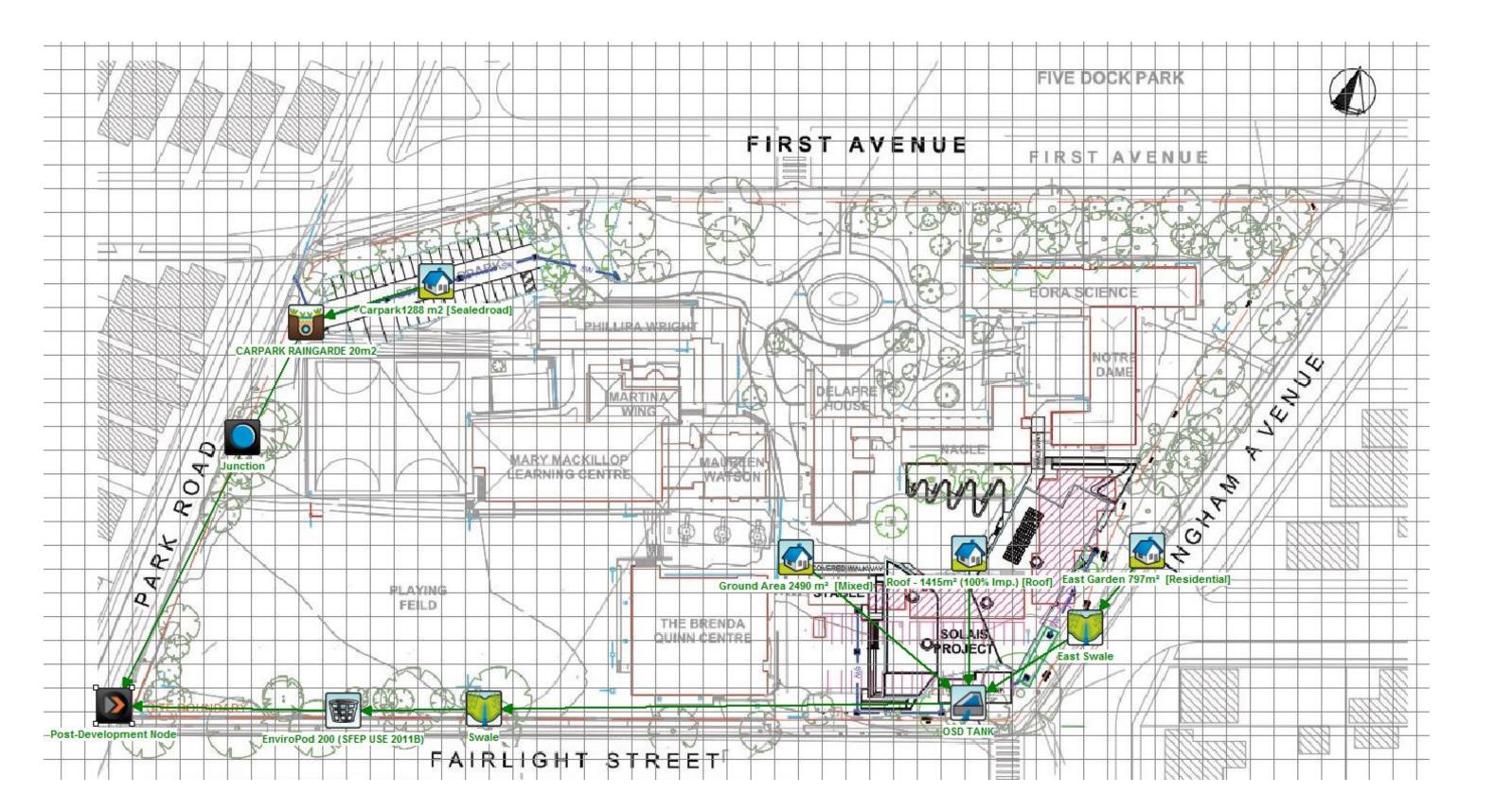
Measure	Location	Purpose
Sediment Fence	Near site boundary along the downstream side of the site.	To prevent sediment leaving the site with stormwater runoff. Stormwater will pass through the fence but the fence will trap the sediment.
Shaker Grid and Wash Down	At construction exit from the site.	To remove ground materials from the construction vehicle wheels prior to the vehicle leaving the site and discharging material onto the public roadway.
Sand Bag Sediment Traps	Directly upstream of all stormwater kerb inlet structures located in close proximity of the site.	To prevent sediment discharged from the site from entering the stormwater inlet structure and contaminating the water course.
Inlet Sediment Trap	Around any stormwater surface inlet structures	To prevent sediment discharged from the site from entering the stormwater inlet structure and contaminating the water course.
Sediment Basin	At the downstream end of the site near the boundary.	To store sediment on site during the construction phase. Basins to be cleaned out prior to the completion of the landscaping in the basins.

Erosion and sediment control will also be further addressed during detailed design and construction of this phase and future development.

Final details of Erosion and Sediment Control measures for the early works and main works to be implemented on site by the successful contractor. The Contractor will be required to take into account the site works staging including the preferred site access points, site shed locations and temporary stockpile locations in developing and implementing these requirements but will be ultimately responsible for managing temporary stormwater and sediment and erosion control during construction.

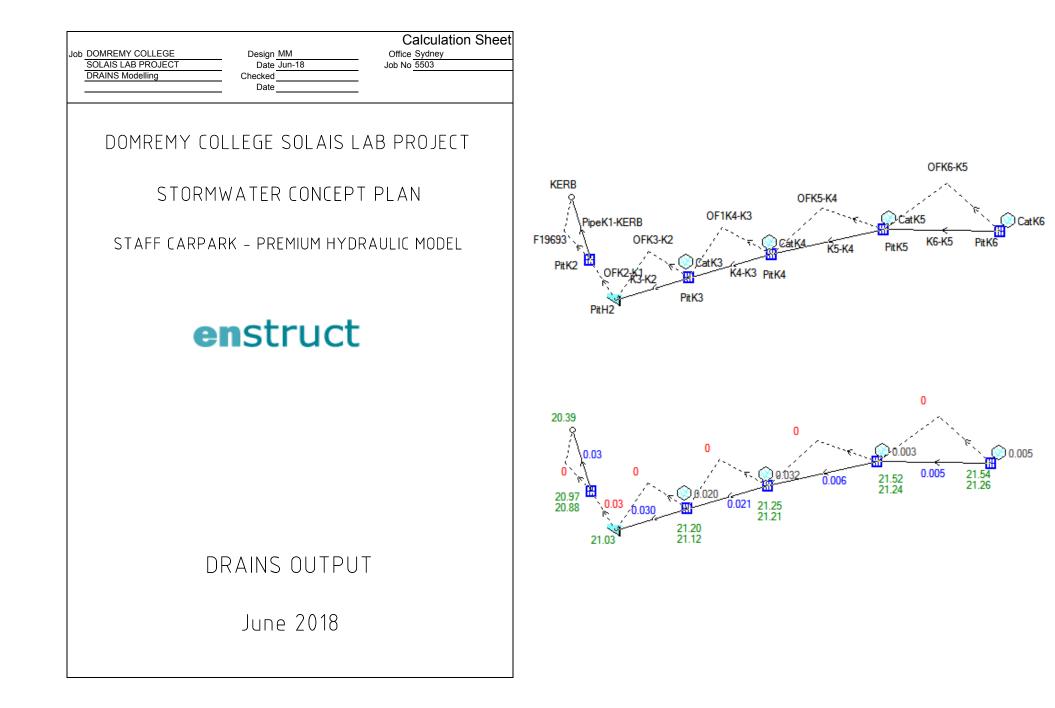












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			Time	Level		Coeff. C	Section		r Minor Storr			Contributing			+	+	\vdash	·'		,	
			(min)	(m)	(m)			(m)		(sq.m/sec)		%		1	+		\downarrow	·'	I	,	
OFF6-F5	PitH6	PitH5	0.1		1		4 m wide pathway	0.3				0	362789					·'		L	
DFF5-F4	PitH5	PitH4	0.1		1		4 m wide pathway	0.3					362789					·'		L	
OF1F4-F3	PitH4	PitH3	0.3			1	4 m wide pathway	0.3					362790					·'		L	
DFF3-F2	PitH3	PitH2	0.1				4 m wide pathway	0.3					362790					·			
OFF2-F1	PitH2	PitF2	0.1	2	1 3.6	5 1.96	6 4 m wide pathway	0.3	8 0.15			0	362793				4				
OF19693	PitF2	KERB	0.1				4 m wide pathway	0.3	3 0.15	i 0.4			362795	4 21.	1 20.25						

PROJECT

DOMREMY COLLEGE SOLAIS LAB PROJECT

PROJECT DOMREMY COLLEGE SOLAIS LAB PROJECT

InstructTITLE20 YEAR ARI - RESULTSJOB No5503PREPAREDERDATE19/06/2018CHECKED0DATE0/01/1900

DRAINS File Path:		P:\j1-5500\5503\00 - Ens	truct Documents\0.3 -	Analysis\Civil\OSD\DRA	INS\CARPARK	(
DRAINS Version:		DRAINS Version 2017.1		,									
Modeller's Name:		Miques Moreno											
Description:		CAR PARK Area											
DRAINS results prepared from Version 2018.01													
PIT / NODE DETAILS				Version 8						R	ESULTS		
Name	Max HGL	Max Pond	Max Surface	Max Pond	Min	Overflow	Constraint						
		HGL	Flow Arriving	Volume	Freeboard	(cu.m/s)				5	% AEP		
			(cu.m/s)	(cu.m)	(m)	(***********							
PitH6	21.26	21.54		\	()		0 Inlet Capacity	(
PitH5	21.24	21.52	0.004				0 Inlet Capacity						
PitH4	21.21	21.25					0 Outlet System						
PitH3	21.12	21.2					0 Inlet Capacity						
PitF2	20.88	20.97	0.031	0.4			0 Inlet Capacity	,					
KERB	20.39	20.07	0.001	0	5.02		- not suparity	1					
	20.33		0		1		-						
SUB-CATCHMENT DETAILS					1		-						
Name	Max	Paved	Grassed	Paved	Grassed	Supp.	Due to Storm						
		Max Q	Max Q	Tc	Tc	Тс	240 10 010111						
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)							
CatH6	0.005	0.005	(60.11/3)	(11111)	5 5		5 5% AEP, 5 m	in hurst Storm	1				
CatH5	0.003	0.003	0	F	-		5 5% AEP, 5 m						
CatH4	0.003	0.003	0	,			5 5% AEP, 5 m						
CatH3	0.032	0.032					5 5% AEP, 5 m						
	0.02	0.02	0	, , , , , , , , , , , , , , , , , , ,	, J	'	5 5 % ALF, 5 m	in burst, Storm	' 				
							-						
PIPE DETAILS							-						
Name	Max Q	Max V	Max U/S	Max D/S	Due to Storm								
Name		(m/s)	HGL (m)	HGL (m)	Due to Storm								
F6-F5	· /	\		()	2 5% AEP, 5 m	in hurst Ctor							
F5-F4	0.005	0.29			5% AEP, 5 m 5% AEP, 15 r								
F3-F4	0.006	0.50			5% AEP, 151 5% AEP, 15 r								
F4-F3 F3-F2	0.021	0.52			5% AEP, 15 r 5% AEP, 20 r								
PipeF1-KERB	0.03	1.72	20.585	20.394	5% AEP, 20 r	nin durst, Sto	rm 8						
							+		↓↓				
CHANNEL DETAILS							+		↓↓				
Name		Max V			Due to Storm		+		↓↓				
	(cu.m/s)	(m/s)					+		↓↓				
OVERFLOW ROUTE DETAILS								-					
Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm					
OFF6-F5	0	0	0.908		0 0		U 0)					
OFF5-F4	0	0	1.268		0		0 0						
OF1F4-F3	0		0.743		-		0 0						
OFF3-F2	0	0	0.589	(, 0		0 0						
OFF2-F1	0.03	0.03	0.908						nin burst, Storm	4			
OF19693	0	0	0.908	0	0 0		0 0						

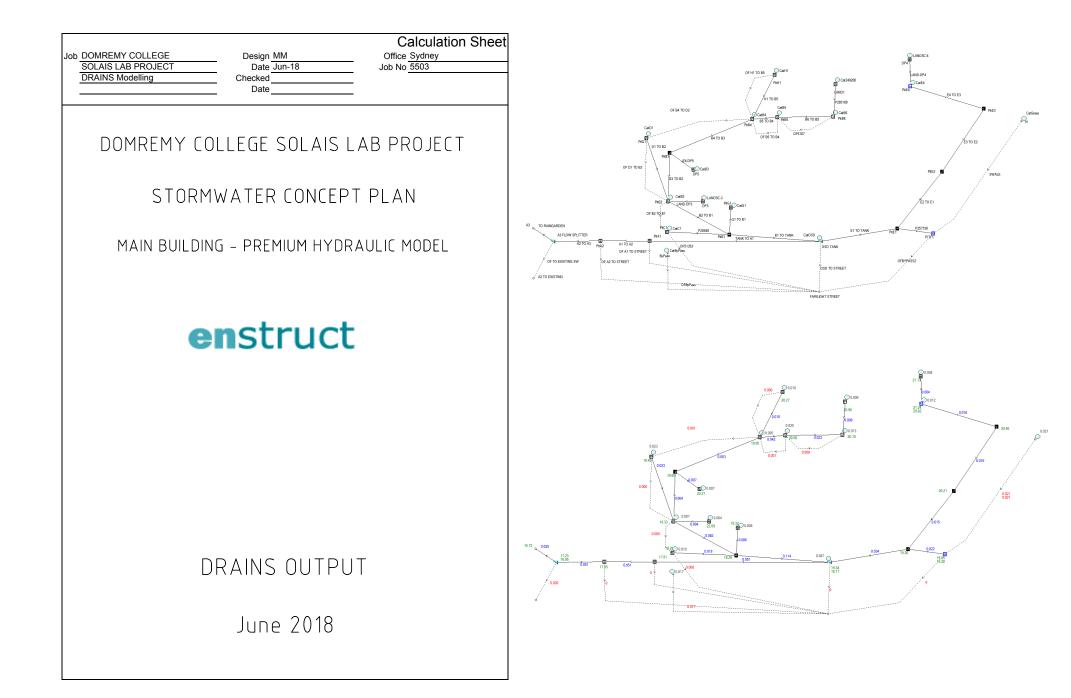
DETENTION BASIN DETAILS									
Name	Max WL	MaxVol	Max Q	Max Q	Max Q				
			Total	Low Level	High Level				
PitH2	21.03	1.2	0.03	C	0.03	5			
Run Log for CARPARK run at 18:30:42 on 19/6/2018									
The maximum water level in these storages exceeds the maximum e	elevation you sp	pecified: PitH2.							
DRAINS has extrapolated the Elevation vs Storage table to a higher	Elevation. Ple	ase provide accurate valu	es for higher elevation	S.					
No water upwelling from any pit.									
Freeboard was less than 0.15m at PitF2, PitH3, PitH4									
Flows were safe in all overflow routes.									
IGNORE THESE WARNINGS AT YOUR OWN PERIL.\cf1									

PROJECT DOMREMY COLLEGE SOLAIS LAB PROJECT

InstructTitle20 YEAR ARI - RESULTSJOB No5503PREPAREDMMDATE19/06/2018CHECKED0DATE0/01/1900

DRAINS File Path:		P:\j1-5500\5503\00 - En:	struct Documents\0.3	- Analysis\Civil\OSD\DR	AINS\CARPARI	<						
DRAINS Version:		DRAINS Version 2017.1		. ,								
Modeller's Name:		Migueas Moreno	1 20 000 2011									
Description:		CAR PARK Area										
DRAINS results prepared from Version 2018.01		0/411/441/404										
					1							
PIT / NODE DETAILS				Version 8						R	ESULTS	S i
Name	Max HGL	Max Pond	Max Surface	Max Pond	Min	Overflow	Constraint					
Tranic	Midx TIGE	HGL	Flow Arriving	Volume	Freeboard	(cu.m/s)	Constraint				1% AEP	
		HOL .	(cu.m/s)	(cu.m)	(m)	(00.1170)						
PitH6	21.32	21.55			.1 0.19	3	0 Inlet Capacity					
PitH5	21.22	21.52			.3 0.22		0 Inlet Capacity					
PitH4	21.23	21.3			1 (0 Outlet System					
PitH3	21.23	21.21			.5 0.0		0 Inlet Capacity					
PitF2	20.94	21.01			.8 (0 Outlet System					
KERB	20.39	21.01		4 C	.0 (, 	o Guiler Gystell				+ +	
	20.39					+					+ +	
SUB-CATCHMENT DETAILS								1			+ +	
Name	Max	Paved	Grassed	Paved	Grassed	Supp.	Due to Storm				+ +	
Inditio	Flow Q	Max Q	Max Q	Tc	Tc	Tc		1			+ +	
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)					+ +	
CatH6	0.007	0.007	· /	0	5 5		5 1% AEP, 5 m	in hurst Storm	1		+ +	
CatH5	0.007	0.004		0	5 5		5 1% AEP, 5 m				+ +	
CatH4	0.004	0.042		0	5 5		5 1% AEP, 5 m					
CatH3	0.042	0.042		0	5 5		5 1% AEP, 5 m					
Cains	0.026	0.026		0	5 3	0	5 1% AEP, 5 III	in burst, Storm	1			
					_							
					_							
PIPE DETAILS	May 0	M>/	March 11/0	Mari D/O	Due to Oteres							
Name	Max Q	Max V	Max U/S	Max D/S	Due to Storm							
F0 F5	(cu.m/s)	(m/s)	HGL (m)	HGL (m)			ļ					
F6-F5	0.007	0.37			16 1% AEP, 5 m							
F5-F4	0.008	0.44			31 1% AEP, 20							
F4-F3	0.021	0.53			35 1% AEP, 10							
F3-F2	0.033	0.83			28 1% AEP, 20							
PipeF1-KERB	0.032	1.8	20.60	5 20.3	95 1% AEP, 20	min burst, Sto	rm 4					
						+					+	
CHANNEL DETAILS				-		+					+	
Name	Max Q	Max V		-	Due to Storm						+	
	(cu.m/s)	(m/s)										
OVERFLOW ROUTE DETAILS		N 0.5/2										
Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm				
OFF6-F5	0	(1.47	-	0 0	-	0 0					
OFF5-F4	0	(0 (0 0					
OF1F4-F3	0	(1.10		0 (0 0					
OFF3-F2	0	(1.50		0 (0 0					
OFF2-F1	0.032	0.032							nin burst, Storm	18		
OF19693		(1.47	01	0 0	1	0 0	1	1		1 1	

DETENTION BASIN DETAILS									
Name	Max WL	MaxVol	Max Q	Max Q	Max Q				
			Total	Low Level	High Level				
PitH2	21.03	1.2	0.032	0	0.032				
Run Log for CARPARK run at 18:28:14 on 19/6/2018									
The maximum water level in these storages exceeds the maximum e	elevation you sp	ecified: PitH2.							
DRAINS has extrapolated the Elevation vs Storage table to a higher	Elevation. Plea	ase provide accurate valu	es for higher elevation	S.					
No water upwelling from any pit.									
Freeboard was less than 0.15m at PitF2, PitH3, PitH4									
Flows were safe in all overflow routes.									
IGNORE THESE WARNINGS AT YOUR OWN PERIL.\cf1									



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DRAINS File Path: DRAINS Version:		P:\j1-5500\5503\00 - Enstruct Docum DRAINS Version 2017.11 - 26 Oct 20		vil\OSD\DRAIN	NS/MAINBUILDING3						_					
Modeller's Name:		Miqueas Moreno	017								_					
Description:		Main Building Area									-					
PIT / NODE DETAILS			Version 13													
Name	Туре	Family	Size	Ponding	Pressure Surfac	Max Pond	Base	Blocking	x y Bolt-dow	n id Part Full	Inflow	Pit is				
				Volume	Change Elev (n		Inflow	Factor	lid		ss Hydrograp					
				(cu.m)	Coeff. Ku		(cu.m/s)									
PitD1	OnGrade	Grated Drain	0.2X4 m		5.9 2	.03		0 0.3	3 579.28 -1241.68 No	17780 1 x Ku	No	New				
PitB2	OnGrade	GD	900sqm			.87		0 0.3		17777 1 x Ku	No	New				
PitB1	OnGrade	Junction Pit or Manhole (seal				9.3		0 0.3		17784 1 x Ku	No	New				
PitA1 PitA2	OnGrade OnGrade	GRATE P-50 PITS Junction Pit or Manhole (seal	450x600 GRATE			.68		0 0.3		159067 1 x Ku 15048256 1 x Ku	No No	New New				
A3	Node	Junction Pit or Manhole (seal	JUNCTION PILOT IN	annoie	1.0 1	.00		0 0.3	24.88 -1680.88	10602706	No	INEW				
FAIRLIGHT STREET	Node					8.8		0	1424.56 -1991.92	76349	No					
A2 TO EXISTING	Node			-		16		0	26.32 -1925.68	159257	No					
PitH1	OnGrade	GD	900sqm		5.9 2	.91		0 0.3		2073213 1 x Ku	No	New				
PitB4	OnGrade	GRATE P-50 PITS	900SQ GRATE F	2-30		0.5		0 0.3		17773 1 x Ku	No	New				
PitB3	OnGrade	Junction Pit or Manhole (seal				0.2		0 0.3	3 693.04 -1312.24 Yes	76294 1 x Ku	No	New				
N	Node					.95		0	2415.28 -1156.72	2815622	No					
DP3	OnGrade	Downpipe	Downpipe		5.9 2	.95		0 0.3	3 856 -1551 No	4955609 1 x Ku	No	New				
DP4	OnGrade	Grated Drain	0.2X4 m		5.9 22.1.2			0 0.3	3 1868.08 -857.2 No	4955635 1 x Ku	No	New				
PitE4	Sag	GRATE P-50 PITS	900SQ GRATE F			.22 0.1	05	0 0.5		17858 1 x Ku	No	New				
PitE3	OnGrade	Junction Pit or Manhole (seal				.14		0 0.3		17865 1 x Ku	No	New				
PitE2	OnGrade	Junction Pit or Manhole (seal				0.9		0 0.3	3 2026.48 -1404.4 Yes	76308 1 x Ku	No	New	I			
PitE1	OnGrade	Junction Pit or Manhole (seal		anhole		0.9	_	0 0.3		76338 1 x Ku	No	New	1		+ $+$ $+$	
PitG1 PitC1	OnGrade OnGrade	Grated Drain Grated Drain	0.2X4 m 0.2X4 m		5.6	20		0 0.3		4955756 1 x Ku 4955791 1 x Ku	No No	New New	I			
		Grated Drain	0.274 11	_				0 0.3		5081041		INEW				
ByPass DP5	Node OnGrade	Downnine	Downning	1		.59		0 0.3		9212520 1 x Ku	No No	New	1			
PITF1	Sag	Downpipe GRATE P-50 PITS	Downpipe 600SQ GRATE F				.1	0 0.5		13231375 1 x Ku	No	New	-			
LAND1	OnGrade	Downpipe	Downpipe	1		.25		0 0.3	3 1506.4 -977.2 No	14136333 1 x Ku	No	New	1			
PitB6	OnGrade	GD	1200sqm	1	0 2	.72		0 0.3		17706 1 x Ku	No	New	1			1
PitB5	OnGrade	GD	900sqm	1		.65		0 0.0		17717 1 x Ku	No	New	1			
		-		1							1.2		1			
DETENTION BASIN DETAILS				1												
Name	Elev	Surf. Area	Not Used	Outlet Typ	K Dia(mr	i) Centre RL		ily Pit Type	x y HED	Crest RL Crest Len	igthid					
OSD TANK	17.3			Orifice		152 17			1433.2 -1745.68 Yes	18.75	4 17468	В				
	17.44															
	17.45															
L	19.15	53	8	1							_	1				
<u> </u>	19.16	1							+ + +			-	I			
	19.6	1														
A3 FLOW SPLITTER	16.87			Orifice		150 16.98	25		124.24 -1745.68 No		10602645	5				
	17.4	I														
SUB-CATCHMENT DETAILS																
Name	Pit or	Total	Paved	Grass	Supp Paved	Grass	Supp	Paved	Grass Supp Paved	Grass Supp	Paved	Grass	Supp	Lag Time	Gutter Gutter G	utter Rainfall
Humo	Node	Area	Area	Area	Area Time	Time	Time	Length	Length Length Slope(%) Slope Slope	Rough	Rough	Rough	or Factor		owFactorMultiplier
		(ha)	%	%	% (min)	(min)	(min)	(m)	(m) (m) %	% %					(m) %	
CatD1	PitD1	0.0368	8 100	0	0 0	5	5	5						0		
CatB2	PitB2	0.0121	95	5	5 0	5	10	5						0		
CatOSD	OSD TANK	0.1416	5 100	0 0	0 0	5	5	5						0		
CatH1	PitH1	0.0163				5	5	5						0		
CatB4	PitB4	0.0084				5	5	5			_	1		0		
CatGrass	N			5 9	51 0	5		5	1 1 1	1 1	1	1	1	0		
LANDSC-3		0.0595					12									
	DP3	0.0094	10	9 9			10	5						0		
LANDSC-4	DP3 DP4	0.0094	10 100) 91 0 1	0 0		10 10	5						0		
LANDSC-4 CatE4	DP3 DP4 PitE4	0.0094 0.007 0.0204	10 100 87.5	0 91 0 0	0 0 0 0 5 0	5	10 10 5	5 5 5						0		
LANDSC-4 CatE4 CatG1	DP3 DP4 PitE4 PitG1	0.0094 0.007 0.0204 0.0093	100 100 8 87.5 8 100	0 91 0 1 5 12.3	0 0	5	10 10 5 5	5 5 5 5						000000000000000000000000000000000000000		
LANDSC-4 CatE4 CatG1 CatC1	DP3 DP4 PitE4 PitG1 PitC1	0.0094 0.007 0.0204 0.0093 0.0302	100 100 87.5 8 100 2 100	0 90 0 0 5 12.8 0 0	0 0 0 0 5 0 0 0 0 0	5 5 5 5	10 10 5 5 5	5 5 5 5 5						0		
LANDSC-4 CatE4 CatG1 CatC1 CatByPass	DP3 DP4 PitE4 PitE1 PitG1 PitG1 PitG1 ByPass	0.0094 0.007 0.0204 0.0093 0.0302 0.0302 0.0423	100 100 87.5 8 100 2 100 8 20	0 90 0 0 5 12.3 0 0 0 0 80 0 80	0 0 0 0 5 0 0 0 0 0	5 5 5 5	10 5 5 5 10	5 5 5 5 5 5 5 5 5						0		
LANDSC-4 CatE4 CatG1 CatC1 CatByPass CatB3	DP3 DP4 PitE4 PitG1 PitG1 PitC1 ByPass DP5	0.0094 0.007 0.0204 0.0093 0.0302 0.0423 0.0423 0.0108	100 87.5 100 100 100 100 100 100 100	0 99 5 12.3 0 0 0 0 0 0 0 80 0 0 0	0 0 0 0 5 0 0 0 0 0	5 5 5 5	10 10 5 5 5	5 5 5 5 5 5 5 5 5 5 5 5 5						000000000000000000000000000000000000000		
LANDSC-4 CatE4 CatC1 CatB3 CatB3 CatB3 CatB3 CatB3 CatB3	DP3 DP4 PRE4 PRG1 PRG1 PRC1 ByPass DP5 LAND1	0.0094 0.007 0.0204 0.0093 0.0302 0.0423 0.0423 0.0105 0.0155	10 100 87.5 100 100 2 100 2 100 3 20 3 100 9 90 90	0 99 0 12.3 0 12.3 0 10 0 10 0 89 0 11	0 0 0 0 5 0 0 0 0 0 0 0 0 0 0 0	5 5 5 5	10 5 5 5 10	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5						000000000000000000000000000000000000000		
LANDSC-4 CatE4 CatG1 CatC1 CatByPass CatB3	DP3 DP4 PitE4 PitG1 PitG1 PitC1 ByPass DP5	0.0094 0.007 0.0204 0.0093 0.0302 0.0423 0.0423 0.0108	100 87.5 100 100 100 100 100 100 100 100 100 10	0 9i 0 0 5 12.3 0 0 0 0 0 0 0 0 0 10 0 11 0 11	0 0 0 0 5 0 0 0 0 0 0 0 0 0 0 0	5 5 5 5	10 5 5 5 10	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5								
LANDSC-4 CatE4 CatG1 CatByPass CatByPass CatByAss CatBA CatBA <	DP3 DP4 PitE4 PitG1 PitG1 PitG1 ByPass DP5 LAND1 PitB6	0.004 0.007 0.0204 0.0032 0.032 0.0423 0.0108 0.0108 0.0152 0.0222	100 87.5 100 100 100 100 100 100 100 100 100 10	0 9i 0 0 5 12.3 0 0 0 0 0 0 0 0 0 10 0 11 0 11	0 0 0 0 5 0 0 0 0 0 0 0 0 0 0 0	5 5 5 5	10 5 5 5 10	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5								
LANDSC-4 CatE4 CatG1 CatC1 CatByPass CatB3 Cat248200 CatB6	DP3 DP4 PitE4 PitG1 PitG1 PitG1 ByPass DP5 LAND1 PitB6	0.004 0.007 0.0204 0.0032 0.032 0.0423 0.0108 0.0108 0.0152 0.0222	100 87.5 100 100 100 100 100 100 100 100 100 10	0 9i 0 0 5 12.3 0 0 0 0 0 0 0 0 0 10 0 11 0 11	0 0 0 0 5 0 0 0 0 0 0 0 0 0 0 0	5 5 5 5	10 5 5 5 10	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5								
LANDSC-4 CatE4 CatG1 CatC1 CatByPass CatByPass CatB3 CatB4200 CatB4200 CatB5 CatB5	DP3 DP4 PitE4 PitG1 PitG1 PitG1 ByPass DP5 LAND1 PitB6	0.004 0.007 0.0204 0.0032 0.032 0.0423 0.0108 0.0108 0.0152 0.0222	100 87.5 100 100 100 100 100 100 100 100 100 10	0 9i 0 0 5 12.3 0 0 0 0 0 0 0 0 0 10 0 11 0 11	0 0 0 0 0 0 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6	10 5 5 5 10	5 5 5 5 5 5 5 5 5 5 5 5 5 1 0 1.D.	Rough Pipe Is No. Pipe	is Chg From At Chg	Chg	RI	Chg			
ANDSC-4 CatE4 CatE4 CatE4 CatE4 CatE4 CatE3 CatE3 CatE3 CatE3 CatE3 CatE3 CatE3 CatE3 CatE5 PIPE DETALS Name <	DP3 DP4 DP4 PitE4 PitE4 PitE1 PitC1 ByPass DP5 LAND1 PitB5 From	0.0094 0.007 0.0204 0.0303 0.0302 0.0423 0.0105 0.0105 0.0222 0.0337 To	11 100 87.5 100 100 100 100 100 100 100 10	0 90 0 0 5 12.3 0 0 0 0 0 10 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11	0 0 0 0 0 0 5 0	6	10 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm)		· · ·	Chg (m)	Ri (m)	Chg (m)			
LANDSC-4 CatE4 CatE4 CatC1 CatC1 CatC1 CatByPass CatB3 CatB3 CatB6 CatB6 CatB5 PIPE DETAILS Name DI TO B2	DP3 DP4 DP4 PitE4 PitE1 PitC1 ByPass DP5 LAND1 PitB5 From From PitD1 PitD1	0.0094 0.007 0.0204 0.0092 0.0092 0.0092 0.0195 0.0195 0.0222 0.0337 To PRB2	11 100 87.1 100 100 100 100 200 90 90 90 90 90 90 90 90 90 90 90 90 9	0 90 0 0 5 12.3 0 0 0 0 0 0 0 0 0 10 0 11 0 12 0 12 0 12	0 0 0 0 0 5 0 0 0 0	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	10 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm) 300 300	0 0.3 New	1 PitD1			Chg (m)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	etc	
ANDSC-4 CatE4 CatE4 CatE4 CatE4 CatE4 CatC1 CatB5 CatB424200 CatB6 CatB5 CatB6 CatB5 PIPE DETAILS Name D1 TO B2 B2 TO B1 D1	DP3 DP4 PitE4 PitE4 PitC1 PitC1 ByPass DP5 LAND1 PitB5 PitB5 From PitD1 PitD2 PitB2	0.0094 0.007 0.0204 0.033 0.0332 0.0423 0.0105 0.0105 0.0222 0.0337 To P#B2 P#B1	111 100 87.5 100 100 100 100 100 100 100 100 100 10	0 90 0 12.1 5 12.1 0 0 0 0 0 0 0 11	0 0 0 0 0 0 5 0 0 0 0 0 0	6 5 5 5 5 7 7 7 7 7 7 7 7 7 7 7 8 3 7 7 7 9 5 5 5 5 5 5 5 5 5 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7	10 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm) 300 300 300 300	0 0.3 New 0 0.3 New	1 PitD1 1 PitB2	(m)		Chg (m)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	etc	
LANDSC 4 CatE4 CatE4 CatC1 CatC1 CatC1 CatByPass CatB3 CatB3 CatB5 CatB5 CatB5 CatB5 CatB5 CatB5 DIPE DETAILS Name DI TO B2 B2 TO B1 B1 TO TANK	DP3 DP4 DP4 PIE4 PIE3 PIG1 PIG1 ByPass DP5 LAND1 PIE66 PIE55 From PIE1 PIE32 PIE31	0.0094 0.007 0.0204 0.0092 0.0422 0.0302 0.0422 0.0412 0.0412 0.0222 0.0337 To Piß2 Piß2 Piß1 OSD TANK	1 11 100 87.5 100 200 200 200 200 200 200 200	D 90 0 1 5 12.5 0 1 0 1 0 1 0 13 0 14 0 18 0 18	0 0 0 0 0 0 5 0 0 0 0 0 0	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	10 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm) 300 300 300 300 375 375	0 0.3 New 0 0.3 New 5 0.3 New 5 0.3 NewFixed	1 PitD1 1 PitB2 1 PitB1	(m) 0 0 0		Chg (m)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	etc	
ANDSC-4 CatE4 CatE5 CatE1 CatE1 CatE3 CatE4 CatE3 CatE4 CatE3 CatE4 CatE4 CatE5 CatE6 CatE6 CatE6 CatE6 CatE7 CatE6 CatE7 CatE6 CatE6 CatE7 D1 TO B2 B2 TO B1 B1 TO TANK TANK TO A1	DP3 DP4 PIE4 PIE51 PRC1 ByPass DP5 LAND1 PIB5 From PIE11 PIE21 PIE31	0.0094 0.007 0.0204 0.0302 0.0302 0.0423 0.0105 0.0105 0.0222 0.0337 To PIB2 PIB1 OSD TANK PIA1	1 11 100 87.5 100 100 100 100 100 100 100 100 100 10	0 90 0 0 0 0 0 0 0 0 0 0 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 1 17.33	0 0 0 0 0 0 5 0 0 0 0 0 0	6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	10 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm) 800 300 800 300 875 375 225 225	0 0.3 New 0 0.3 New 5 0.3 New 5 0.3 NewFixed 5 0.3 NewFixed	1 PitD1 1 PitB2 1 PitB1 1 OSD TANK	(m)		Chg (m)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	etc	
LANDSC-4 CatE4 CatG1 CatG1 CatG1 CatG1 CatG1 CatB3 CatB4 CatB5 PIPE DETAILS Name D1 TO B2 B1 TO TANK TANK TO A1 A1 TO A2	DP3 DP4 DP4 PIE4 PIE3 PIE3 DP5 DP5 LAND1 PIE86 PIE85 PIE85 From PIE01 PIE31 OSD TANK PIE41 PIE41	0.0094 0.007 0.0204 0.0002 0.0002 0.0022 0.00022 0.0105 0.0105 0.0105 0.0105 0.0105 0.000000	l 110 100 87.5 100 200 200 200 200 200 200 200 200 200	D 90 D 0 D 0 D 12.2 D 1 D 0 D 10 D 11 D 11 V/S IL (m) Q 18.9 9 18.5 1 17.3 0 17.1	0 0 0 0 0 0 5 0 0 0 0 0 0 0 10 12 0 10	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	10 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm) 300 300 300 300 375 375 225 225 225 225	0 0.3 New 0 0.3 New 5 0.3 NewFixed 5 0.3 NewFixed 5 0.3 NewFixed 5 0.3 New	1 PitD1 1 PitB2 1 PitB1 1 OSD TANK 1 PitA1	(m) 0 0 0 0 0		Chg (m)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	etc	
ANDSC-4 CatE4 CatE3 CatE4 CatE3 CatE4 CatE3 CatE4 CatE3 CatE4 CatE3 CatE4 CatE4 CatE4 CatE4 CatE5 CatE6 CatE7 CatE6 CatE7 CatE8 D1 TO B2 B2 TO B1 B1 TO TANK TANK TO A1 A1 TO A2 A2 TO A3	DP3 DP4 PHE4 PHG1 PHG1 ByPass DP5 LAND1 PHB6 PHB5 From PHD1 PHB2 PHD1 PHB4 PHD5 PHB4	0.0094 0.007 0.0204 0.00302 0.0302 0.0423 0.0155 0.0222 0.0155 0.0222 0.0337 To PHB2 PHB1 OSD TANK PHA1 PHA2 PHA1 PHA2 A3 FLOW SPLITTER	1 11 100 107 107 100 100 100 20 100 20 20 100 20 20 20 20 20 20 20 20 20	D 90 D 1 D 1 D 1 D 10 D 10 D 11 D 17.1 V 16.9	0 0 0 0 0 0 5 0 0 0 0 0 0	6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	10 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm) 300 300 300 300 375 375 225 225 225 225 225 225	0 0.3 New 0 0.3 New 5 0.3 NewFixed 5 0.3 NewFixed 5 0.3 NewFixed 5 0.3 NewFixed	1 PitD1 1 PitB2 1 PitB1 1 OSD TANK 1 PitA1 1 PitA2	(m) 0 0 0 0 0 0 0		Chg (m)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	etc	
ANDSC-4 CatE4 CatG1 CatG1 CatG1 CatG1 CatG1 CatG1 CatG1 CatG1 CatG1 CatG2 CatG3 CatG3 CatG3 CatG4 CatG5 PIPE DETAILS Name D1 TO B2 B2 TO B1 B1 TO TANK TANK TO A1 A1 TO A2 A2 TO A3 TO RAINGARDEN	DP3 DP4 PRE4 PR01 PR01 BVP38 DP45 DP45 LAND1 PR06 PR05 DP5 LAND1 PR06 PR05 DP5 PR05 DP5 PR05 DP5 PR05 DP5 PR05 DP6 PR07 PR07 PR01 PR07 PR01 PR07 PR05 PR07 PR07 PR07	0.0094 0.007 0.0204 0.003 0.0302 0.0422 0.0422 0.0422 0.0108 0.0158 0.0337 To PRB2 PRB1 PRB1 PRB1 PRB1 PRA2 PRA1 PRA2 A3 FLOW SPLITTER A3	Length (m) 122 (m) 100 (m) 100	0 90 0 0 0 0 0 12.2 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 11 10 11 11 17.3 0 17.1 4 16.8	0 0 0 0 0 0 5 0 0 0 0 0 0	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	10 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm) 300 300 300 300 375 375 225 225 225 225 225 225 150 150	0 0.3 New 0 0.3 New 5 0.3 NewFixed 5 0.3 NewFixed 5 0.3 NewFixed 5 0.3 NewFixed 0 0.3 NewFixed	1 PitD1 1 PitB2 1 PitB1 1 OSD TANK 1 PitA1 1 PitA2 1 A3 FLOW \$	(m) 0 0 0 0 0		Chg (m)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	etc	
ANDSC-4 CatE4 CatE3 CatE4 CatE3 CatE4 CatE3 CatE3 CatE3 CatE3 CatE4 CatE3 CatE4 CatE4 CatE4 CatE5 CatE6 CatB5 CatB5 PIPE DETAILS Name D1 TO B2 B2 TO B1 B1 TO TANK TANK TO A1 A1 TO A2 A2 TO A3	DP3 DP4 PHE4 PHG1 PHG1 ByPass DP5 LAND1 PHB6 PHB5 From PHD1 PHB2 PHD1 PHB4 PHD5 PHB4	0.0094 0.007 0.0204 0.00302 0.0302 0.0423 0.0155 0.0222 0.0155 0.0222 0.0337 To PHB2 PHB1 OSD TANK PHA1 PHA2 PHA1 PHA2 A3 FLOW SPLITTER	1 11 100 107 107 100 100 100 20 100 20 20 100 20 20 20 20 20 20 20 20 20	D 90 D 0 D 0 D 10 D 11 D 17.1.1 4 16.8 8 20.1	0 0 0 0 0 0 5 0 0 0 17.14 (16.99) 9 16.657 7 16.656 (0 2.004 (16.65) 0 2.00	6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	10 5 5 5 5 5 5 5 5 5 5 5 5 5	(mm) 300 300 300 300 375 375 225 225 225 225 225 225	0 0.3 New 0 0.3 New 5 0.3 NewFixed 5 0.3 NewFixed 5 0.3 NewFixed 5 0.3 NewFixed 0 0.3 NewFixed 0 0.3 NewFixed 0 0.3 New	1 PitD1 1 PitB2 1 PitB1 1 OSD TANK 1 PitA1 1 PitA2	(m) 0 0 0 0 0 0 0		Chg (m)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	etc	

PROJECT DOMREMY COLLEGE SOLAIS LAB PROJECT

TITLE

JOB NO DRAINS DATA - DEVELOPED (WITH OSD) SCENARIO PREPARED CHECKED

MM 0 5503 DATE DATE

AMD GPAPH	LAND-DP3	DP3	PitB2	1	22	19.12	20.0	Concrete, under roads, 1% minimum slope	100	100	0.2	Now	1	DP3	0	1	1	1		
G4 TO G3.PHEG				40.2											0					
Bit3PH3															0					
B210 P82															0					
E110 ANM PME1 OSD TAMK PME1 1817 1817 1817 1815 1050 Some model wash, Nimmirum alog 190 300 0.3 New 1 PME1 0<															0					
G1 TO B1 PIB1 10 122 100 122 100 122 100 122 100 122 100 122 100 122 100 <															0					
P2040PAC1PAC1PAC1PAC1OCC </td <td></td> <td></td> <td></td> <td>10.1</td> <td></td> <td>0</td> <td></td> <td></td> <td></td> <td></td> <td></td>				10.1											0					
EX-DPS DPS DPS DPS D DPS D															0					
P257193 PTT-1 PdE 1 <				1											0					
P2859 LAND1 P189 P7.2 D30 P1.9 P1.9 P1.9 P1.9															0					
Bit DB 5 PIB6 PIB6 PIB7 PIB8 PIB7 PIB8 PIB7 PIB8 PIB8 PIB8 PIB8 <				-											0				 	
BBT De A PRBS PRSS PRSS PRSS PRSS <															0				 	
Deplex OPINE of Services CR0SING OPINE of Services CR0															0				 	
Pipe Chg Bottom Height of Serve Ch Bottom Height of Serve Rot Height of Serve Rot Rot <td>B5 TO B4</td> <td>PItB5</td> <td>PItB4</td> <td>10.</td> <td>2 19.88</td> <td>19.75</td> <td>1.27</td> <td>Concrete, not under roads, 0.5% minimum sid</td> <td>300</td> <td>300</td> <td>0.3</td> <td>New</td> <td>1</td> <td>PItB5</td> <td>0</td> <td></td> <td></td> <td></td> <td> </td> <td></td>	B5 TO B4	PItB5	PItB4	10.	2 19.88	19.75	1.27	Concrete, not under roads, 0.5% minimum sid	300	300	0.3	New	1	PItB5	0				 	
Pipe Chg Bottom Height of Serve Ch Bottom Height of Serve Rot Height of Serve Rot Rot <td></td>																				
Image Image <th< td=""><td></td><td></td><td>-</td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>			-		-															
CHANNEL DTAILS Check Construction	Pipe				Chg															
Name From Type Length U/S IL D/S IL Blope Base Wirth Le. Slope R.B. Slope Manne Depth Rolf D <thd< th=""> D <thd< td=""><td></td><td>(m)</td><td>Elev (m)</td><td>(m)</td><td>(m)</td><td>Elev (m)</td><td>(m)</td><td>(m)</td><td>Elev (m)</td><td>(m) e</td><td>etc</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></thd<></thd<>		(m)	Elev (m)	(m)	(m)	Elev (m)	(m)	(m)	Elev (m)	(m) e	etc									
Name From Type Length U/S IL D/S IL Blope Base Wirth Le. Slope R.B. Slope Manne Depth Rolf D <thd< th=""> D <thd< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></thd<></thd<>																				
Image Image <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>								-												
OPERFLOW ROUTE DETAILS OP OP<	Name	From	То	Туре	Length							Manning	Depth	Roofed						
Name From To Travel Spill Crest War Cross Safe Depth SafeDepth Safe					(m)	(m)	(m)	(%)	(m)	(1:?) ((1:?)	n	(m)							
Name From To Tavel Spill Crest War Cross Safe Depth SafeDepth Safe Bed D/S Area id U/S IL D/S IL Length Cold Main Safe Bed D/S Area id U/S IL D/S IL Length Cold Main Safe Bed D/S Area id U/S IL D/S IL Length Cold Main 0 F D1 TO EX PHD1 PHB2 0.1 Cold A m wide pathway 0.3 0.15 0.4 3 0 19.03 19.42 15 0																				
Image Image Length Coeff. C Section Major Sion Minor Store (More Store) Contributing Contributing <thcontributing< th=""> Contributing</thcontributing<>																				
CF D1 TO B2 PID1 PHB2 D1 4 m wide pathway 0.3 0.15 0.4 8 0 78342 0.01 9.42 0.01	Name	From	То											id	U	/S IL	D/S IL Len	gth (m)		
OF D 11 D B2 PHD1 PHB2 0.1 4 m wide pathway 0.3 0.1 0.4 8 0 76342 20.3 9.12 13 13 13 13 14 <td></td> <td></td> <td></td> <td>Time</td> <td>Level</td> <td>Length</td> <td>Coeff. C</td> <td>Section</td> <td>Major Storr</td> <td></td> <td></td> <td></td> <td>Contributi</td> <td>ng</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>				Time	Level	Length	Coeff. C	Section	Major Storr				Contributi	ng						
OF B2 TO B1 PH62 PH61 0.1 1 4 m wide pathway 0.3 0.1 0.4 3 0 19.87 19.42 15 0 0 OSD TO STREET OSD TANK FARLGHT STREET 0.1 15 4 2.16 wide pathway 0.3 0.15 0.4 20 0 80163 18.2 17 6 0 0 0 19.87 19.42 15 0 0 0 0 80163 16.2 16.2 16.2 0 1653003 19.87 19.42 15 0 0 0 1653003 16.2 17.6 0 0 0 1653003 17.79 17.26 10 0 165003 17.79 17.65 2 0 0 0 1600266 17.34 17.65 2 0 0 1600266 17.34 17.65 2 0 0 1600266 17.34 17.65 2 0 0 1600266 17.34				(min)	(m)	(m)			(m)	(m) ((sq.m/sec)	(%)	%							
OSD TOSTREET OSD TANK FARLIGHT STREET 0.1 19.5 2.15 m wide pathway 0.3 0.15 0.4 2.0 0 8633 18.2 17 6 6 6 6 OF A1 TO STREET PIA1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 159078 19.3 17 6				0.	1				0.3				C					12		
OF A1 TO STREET PIA1 FARLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 159078 19.3 17.7 6 0 0 0F A2 TO STREET PIA2 FARLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 1553003 17.79 17.26 10 0 0F A2 TO STREET PIA2 A2 TO EXISTING 0.1 1 1 0 1650003 17.79 17.26 0 0 0 0 10 10002661 17.34 17.65 2 0 0 0 0 1001 10002661 17.34 17.65 2 0 0 100 10002661 17.34 17.65 2 0 0 1001 0 1001 0 1001 0 1001 0 1701 20.9 20.65 7.83 0 0 100 1001 1001 0 1001 0 1001 1001				0.					0.3			4 3	C				19.42	15		
OF A2 TO STREET PiA2 FARLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 5.4 0 1550031 17.73 17.25 10 0 0 0 OF TO EXISTING A2 TO EXISTING 0.1 17.17 1.06 Channel section 600 mm wide 0.09 0.01 1 0 10602661 17.34 17.25 10 0 0 0 0 1 1 0 1060261 17.34 17.36 12.5 0 0 1 1 0 1060261 17.34 17.55 1 0 0 0 0 1 1 0 1060261 17.34 17.55 1 0 0 15 0 1.31 0 105020 120 4 m wide pathway 0.3 0.15 0.4 3.19 0 17910 20.9 20.55 7.83 0 0 17910 20.9 20.55 7.83 0 0 155 0 17910				0.	1 19.5	4	2.15	4 m wide pathway					0					6		
OF TO EXISTING SW A3 FLOW SPLITTER A2 TO EXISTING 0.1 1 1 0 100 (2061) 17.36 7.65 2 0 0 OF H1 TO B5 PHH PtB4 0.1 4 m wide pathway 0.3 0.15 0.4 3.19 0 17.96 2.9 0.65 7.83 0 0 17.06 2.9 20.65 7.83 0 0 17.90 2.9 20.65 7.83 0 0 1.05 0.4 3.19 0 17.90 2.9 20.65 7.83 0 0 1.05 0.4 3.19 0 17.90 2.9 20.65 7.83 0 0 1.05 0.4 3.19 0 1.05 0.4 3.19 0 1.05 0.4 3.19 0 1.05 0.4 1.4 1.00 1.06 1.4 1.00 1.05 0.4 1.4 1.00 1.05 0.4 1.4 1.00 1.05 0.4 1.4 1.00								4 m wide pathway					C					6		
OF HIT DE5 PHH PHB4 0.1 4 m wide pathway 0.3 0.15 0.4 3.19 0 17910 20.9 20.65 7.83 0 0 OF B4 TO D2 PHB4 PHD1 0.2 4 m wide pathway 0.3 0.15 0.4 3.19 0 17910 20.9 20.65 7.83 0 0 VMLE N PHTF1 2.1 DOMREMY SWALE Goord 0.15 0.4 0.4 100 10474271 20.65 19.5 66 0 OF51353 PHC1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 14.2 0 6901547 19.42 18 10 0 OFBYPASS2 PHT1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 520854 18.59 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0				0.							0.4	5.4	C					10		
OF B4 TO D2 PIB4 PtD1 0.2 4 m wide pathway 0.3 0.15 0.4 2.51 0 78.03 20.5 20.03 25.8 0 0 SWALE N PITF1 2.1 DOMREMY SWALE 600mm 0.15 0.4 1.44 100 10474271 20.65 10.5 0.6 1.44 100 10474271 20.65 10.5 0.6 1.44 100 10474271 20.65 10.5 0.6 1.44 100 10474271 20.65 10.5 0.6 1.44 100 10474271 20.65 10.5 0.6 1.44 100 10.7 10.5 10.5 10.5 10.6 1.44 100 10.7 10.5				0.	1 17.17	1	1.96	Channel section 600 mm wide	0.09		1	1	0	1	0602661			2		
SWALE N PITF1 2.1 DOMREMY SWÁLE 600mm 0.15 0.6 1.44 100 10474271 20.65 19.5 65 OF53333 PIC1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 14.2 0 6901547 19.42 18 10 OF53333 OFBVPASS BVPass FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 5208548 18.59 10 OFBVPASS PITF1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 5208548 18.59 10	OF H1 TO B5			0.	1				0.3	0.15	0.4									
OF51353 PIC1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 14.2 0 6901547 19.42 18 10 0 OF5VPASS ByPass FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 5208548 18.59 10 0 FOR VALUE OFBVPASS2 PIF1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 5208548 18.59 10 0 FOR VALUE FOR VALUE 0 10 12419849 19.5 18.8 10 0 12419849 19.5 18.8 10 0 12419849 19.5 18.8 10 0 12419849 19.5 18.8 10 0 12419849 19.5 18.8 10 0 12419849 19.5 18.8 10 0 12419849 19.5 18.8 10 0 12419849 19.5 18.8 10 0	OF B4 TO D2	PitB4	PitD1	0.	2			4 m wide pathway	0.3	0.15	0.4	2.51	0		76303		20.03	25.8		
OFByPass ByPass FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 5208548 18.59 10 0 0 OFBYPASS2 PITF1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 13419849 19.5 18.8 10 0 1	SWALE	N						DOMREMY SWALE 600mm					100				19.5			
OFBYPASS2 PITF1 FAIRLIGHT STREET 0.1 4 m wide pathway 0.3 0.15 0.4 1 0 13419849 19.5 18.8 10 1	OF51353	PitC1	FAIRLIGHT STREET	0.	1			4 m wide pathway	0.3	0.15	0.4	14.2	C					10		
	OFByPass	ByPass	FAIRLIGHT STREET	0.	1			4 m wide pathway	0.3	0.15	0.4	1	C		5208548	18.59	18.59	10		
	OFBYPASS2	PITF1	FAIRLIGHT STREET	0.	1			4 m wide pathway	0.3	0.15	0.4	1	C	1	3419849	19.5	18.8	10		
	OF5167	PitB6	PitB5	0.	1				0.3	0.15	0.4	0.82	. C		76260	20.72	20.65	8.5		
	OF B5 TO B4	PitB5	PitB4	0.	1				0.3	0.15	0.4	1.47	· C	1	3295321	20.65	20.5	10.2		

PROJECT DOMREMY COLLEGE SOLAIS LAB PROJECT

InstructTITLE20 YEAR ARI - RESULTSJOB No5503PREPAREDERDATE19/06/2018CHECKED0DATE0/01/1900

DRAINS File Path:		P:\j1-5500\5503\00 - Ens	truct Documents\0.3 -	Analvsis\Civil\OSD\DRA	INS\MAINBUIL	DING3				
DRAINS Version:		DRAINS Version 2017.11		.,						
Modeller's Name:		Migueas Moreno								
Description:		Main Building Area								
DRAINS results prepared from Version 2018.01		main Banang , roa								
PIT / NODE DETAILS				Version 8					RE	SULTS
Name	Max HGL	Max Pond	Max Surface	Max Pond	Min	Overflow	Constraint			
	induk FIGE		Flow Arriving	Volume	Freeboard	(cu.m/s)			5`	% AEP
			(cu.m/s)	(cu.m)	(m)	(00				
PitD1	19.43		0.022	()	0.6	5 (0 None			
PitB2	19.17		0.007		0.7		0 None			
PitB1	18.9		0		0.59		None			
PitA1	17.69		0		1.61) None			1
PitA2	17.48		0		0.2		0 None		<u> </u>	
A3	16.73		0		0.2	1			<u> </u>	
PitH1	20.25		0.009		0.66	5 (0 None		<u> </u>	
PitB4	19.93		0.006		0.57		0 None			
PitB3	19.63		0		0.57		None		<u> </u>	
DP3	22.08		0.003		0.87		None			
DP4	21.12		0.004		0.98		None			
PitE4	20.6	21.24	0.012	0.5			Inlet Capacity			
PitE3	20.45		0		0.69		None			
PitE2	20.2		0		0.7		None			
PitE1	18.84		0		2.06		None			
PitG1	19.31		0.005		0.69		None			
PitC1	18.92		0.018		0.5) None			
DP5	22.13		0.006		0.82		None			
PITF1	18.85	19.54	0.018	0.2			0 Inlet Capacity			
LAND1	20.89		0.009		0.36		None			
PitB6	20.07		0.013		0.65	; () None			
PitB5	20.06		0.02		0.59) () None			
SUB-CATCHMENT DETAILS										
Name	Max	Paved	Grassed	Paved	Grassed	Supp.	Due to Storm			
	Flow Q	Max Q	Max Q	Tc	Тс	Тс				
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)				
CatD1	0.017	0.017	0	5	5		5 5% AEP, 5 min burst, Storm			
CatB2	0.005	0.005	0	5	10) :	5 5% AEP, 5 min burst, Storm	1		
CatOSD	0.067	0.067	0	5	5	5	5 5% AEP, 5 min burst, Storm	1		
CatH1	0.007	0.007	0.001	5	5	5 4	5 5% AEP, 15 min burst, Storn	n 10		
CatB4	0.004	0.003	0	5	5	5 .	5 5% AEP, 15 min burst, Storm 10			İ
CatGrass	0.016	0.001	0.015	5	12		5 5% AEP, 15 min burst, Storm 4			
LANDSC-3	0.003	0	0.002	5	10) (5 5% AEP, 15 min burst, Storm 6			
LANDSC-4	0.003	0.003	0	5	10		5 5% AEP, 5 min burst, Storm 1			
CatE4	0.009	0.008	0.001	5	5	5	5 5% AEP, 15 min burst, Storm 10			
CatG1	0.004	0.004	0	5	5	5 4	5 5% AEP, 5 min burst, Storm 1			
CatC1	0.014	0.014	0	5	5	5	5 5% AEP, 5 min burst, Storm 1			
CatByPass	0.012	0.004	0.01	5	10) (5 5% AEP, 15 min burst, Storn			

Constant 0.007	CatB3	0.005	0.005	0	5	5	5	5% AEP. 5 m	in burst, Storm	1			
Calib 0.01 0.00 0.01 0 6 6 6 6 6 8 9 1 <th1< th=""> 1 1 <</th1<>				0.001	5	5						+ +	
GelS 0					-	-						+ +	
PIPE Def MLS Name					5	-						+ +	
Name Carry 					-	-	-					+ +	
Name Mac Dis Mac V Mac V Mac Dis Mac Dis <t< td=""><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td><td>+ +</td><td></td></t<>		-								1		+ +	
Name Carry Carry Carry Di DagName US Carry Carry Di DagName US Carry Di DagName US Di DagN	PIPE DETAILS	-								1		+ +	
Image Image <t< td=""><td></td><td>Max Q</td><td>Max V</td><td>Max U/S</td><td>Max D/S</td><td>Due to Storm</td><td></td><td></td><td></td><td>1</td><td></td><td>+ +</td><td></td></t<>		Max Q	Max V	Max U/S	Max D/S	Due to Storm				1		+ +	
D TO D2 D TO D2 D TO D2 D TO D2 D TO D3 D TO D3 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td><td>+ +</td><td></td></t<>										1		+ +	
Bz TO B1 0.072 3.39 19.042 18.88 9%. APL 71sm hunt. Storm 0 Image: Store	D1 TO B2		· · ·			5% AEP. 5 mi	n burst. Storm	1					
B TO TANK 0.069 0.08 18.833 18.823 94.829 94.89.15 mm bund, Stomm 1 </td <td></td>													
TANK TO A1 0.046 1.21 17.36 17.374<												1	
AT TO A2 0.046 1.15 17.740 77.795 SA EP; 15 mm burd, Storm 4 Imp burd, Storm 1 Imp burd, Storm 1 <t< td=""><td></td><td>0.048</td><td>1.21</td><td>17.95</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>		0.048	1.21	17.95									
A2 TO A3 0.046 1.15 17 A02 77.210 SA AEP, 15 mn burst, Storm 4 Image: Storm 1		0.046											
TO RANGARDEN 0.022 2.65 10.84 10.75 5% AEP. 15 mb burk. Stom 4 0 0 0 BA TO B3 0.048 2.46 18.83 19.6195 % AEP. 5 mb burk. Stom 9 0 0 0 BA TO B2 0.047 2.21 19.522 19.1095 % AEP. 5 mb burk. Stom 9 0 0 0 LAND-DP4 0.003 1.88 22.04 19.725 % AEP. 15 mb burk. Stom 1 0 0 0 EAT DE 2 0.012 2.79 2.045 % AEP. 15 mb burk. Stom 1 0													
H1 TO B5 0.007 0.93 2.21 32.091 95% AEP. 15 mb bars, Storm 1													
B4 TO B3 0.043 2.46 19.83 19.81 P5.82 NEP.5 min burst, Storm 1 Image: Store B Im										† †		1 1	
B3 TO B2 0.047 2.21 19.522 19.192 5%.AEP.15 min burst. Storm 9 Image: Store 1 Image: Store 1 LAND-DP4 0.000 1.48 22.024 19.172 5%.AEP.15 min burst. Storm 1 Image: Store 1 Image: Sto									1	1		1 1	
LAND-DP3 0.003 1.85 22.024 19.172 5% AEP. in burst. Storn 0 Image: Storn 0 Image: Storn 0 E4 T0 E3 0.012 2.79 20.047 20.46 5% AEP. in burst. Storn 10 Image: Storn 0 Image: Storn 0 </td <td></td> <td>0.047</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1 1</td> <td></td>		0.047										1 1	
LNND-0P4 0.003 1.48 21.076 20.684 %k AEP, 5 min burst, Storn 1 Image: Store 1									1	1		1 1	
13 TO E2 0.012 2.5 20.305 KAEP.1 orn hurst. Storm 1 Image: Start S													
E3 TO E2 0.012 2.6 20.396 20.203 5% AEP.1 or m burst. Storm 1 Image: Storm 9									1	1		1 1	
E2 TO E1 0.011 1.07 20.133 19.974 5% AEP, 15 min burst, Storm 4 Image: Constraint of the constraint of	E3 TO E2	0.012	2.5	20.396	20.203	5% AEP, 10 n	nin burst, Storm	n 1					
C1 TO B1 0.004 1.16 19.26 19.06 % AEP. 5 min burst, Storm 1 Image: Store 1 Image		0.011											
C1 TO B1 0.004 1.16 19.26 19.061 % AEP, 5 min burst, Storm 1 Image: Store 1 Imag	E1 TO TANK	0.023	0.9	18.826	18.823	5% AEP, 20 n	nin burst, Storm	n 4					
P20540 0.014 0.06 18.904 18.909 6% AEP. 5 min burst. Storm 1 Image: Constraint of the start of the st	G1 TO B1	0.004	1.16	19.26									
P257158 0.016 0.08 18.841 18.837 (5% AEP, 15 min burst, Storm 1 Image: Constraint of the state of the sta	P20540	0.014	0.36	18.904	18.899	5% AEP, 5 mi	n burst, Storm	1					
P285199 0.007 2.12 20.828 20.073 5% AEP, 15 min burst, Storm 10 Impact Storm 1 I	EX-DP5	0.005	2.23	22.033	19.625	5% AEP, 5 mi	n burst, Storm	1					
B6 TO B5 0.017 0.8 20.073 20.056 3% AEP, 5 min burst, Storm 1 Image	P257158	0.016	0.86	18.841	18.837	5% AEP, 15 n	nin burst, Storm	า 4					
B5 TO B4 0.032 1.57 19.979 19.926 5% AEP, 15 min burst, Storm 9 Image	P285189	0.007	2.12	20.828	20.073	5% AEP, 15 n	nin burst, Storn	n 10				1	
CHANNEL DETAILS Max Q Max V C <thc< th=""> <thc< th=""> C <thc< th=""></thc<></thc<></thc<>	B6 TO B5	0.017	0.8	20.073	20.056	5% AEP, 5 mi	n burst, Storm	1				1	
Name Max Q Max V Due to Storm Image: Color of the state o	B5 TO B4	0.032	1.57	19.979	19.926	5% AEP, 15 n	nin burst, Storm	n 9				1	
Name Max Q Max V Due to Storm Image: Color of the state o													
Image: constraint of the system (constraint of the system)	CHANNEL DETAILS											1	
OVERFLOW ROUTE DETAILS Max Q U/S Max Q D/S Safe Q Max D Max With Max V Due to Storm Image Image <td>Name</td> <td>Max Q</td> <td>Max V</td> <td></td> <td></td> <td>Due to Storm</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	Name	Max Q	Max V			Due to Storm							
Name Max Q U/S Max Q D/S Safe Q Max D Max DV Max Width Max V Due to Storm Image: Constraint of the store of the sto		(cu.m/s)	(m/s)										
Name Max Q U/S Max Q D/S Safe Q Max D Max DV Max Width Max V Due to Storm Image: Constraint of the store of the sto													
OF D1 TO B2 0 0 1.38 0	OVERFLOW ROUTE DETAILS												
OF B2 TO B1 0 0 1.431 0		Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm				
OSD TO STREET 0 0 1.311 0		0	0	1.38	0	0	0	C)				
OF A1 TO STREET 0 0 0.00 0		0	0		0	0	÷						
OF A2 TO STREET 0 0 1.404 0		0	0		9	•	•	-					
OF TO EXISTING SW 0.021 0.021 0.007 0.043 0.02 2.16 0.55 5% AEP, 15 min burst, Storm 4 Implementation OF H1 TO B5 0		0	0		0	0							
OF H1 TO B5 0 0 1.432 0		0	0		0	0	-	-					
OF B4 TO D2 0 0 1.439 0		0.021	0.021		0.043	0.02			5% AEP, 15 r	nin burst, Storm	4		
SWALE 0.016 0.016 0.035 0.08 0.04 0.46 0.51 5% AEP, 15 min burst, Storn 4 0 OF51353 0 <td></td> <td>0</td> <td>0</td> <td></td> <td>°</td> <td>ů</td> <td>-</td> <td>-</td> <td>)</td> <td></td> <td></td> <td></td> <td></td>		0	0		°	ů	-	-)				
OF51353 0 </td <td></td> <td>0</td> <td>0</td> <td></td> <td>0</td> <td>0</td> <td>Ŷ</td> <td>9</td> <td></td> <td></td> <td></td> <td></td> <td></td>		0	0		0	0	Ŷ	9					
OFByPass 0.012 0.012 0.908 0.025 0.01 4 0.3 5% AEP, 15 min burst, Storn 7 OFBYPASS2 0<		0.016	0.016		0.08			0.51	5% AEP, 15 r	nin burst, Storm	4		
OFBYPASS2 0 0 0.908 0 <		0	0		0	ů	-	C	1				
OF5167 0 0 0.822 0 0 0 0 0 0 0		0.012	0.012							nin burst, Storm	7		
		0	°		*	Ů	-	-					
OF B5 TO B4 0 0 1.101 0 0 0 0		0	0		0	ů	-						
	OF B5 TO B4	0	0	1.101	0	0	0	0)				

DETENTION BASIN DETAILS									
Name	Max WL	MaxVol	Max Q	Max Q	Max Q				
			Total	Low Level	High Level				
OSD TANK	18.82	73.1	0.048	0.048	0				
A3 FLOW SPLITTER	17.22	0.3	0.046	0.025	0.021				
Run Log for MAINBUILDING3 run at 18:13:20 on 19/6/2018									
No water upwelling from any pit. Freeboard was adequate at all pits.									
The maximum flow in these overflow routes is unsafe: OF TO EXIST	ING SW								

PROJECT DOMREMY COLLEGE SOLAIS LAB PROJECT

IDB NO5503IDB NO5503PREPAREDMMDATE19/06/2018MMCHECKED0DATE0/01/1900

DRAINS File Path:		P:\j1-5500\5503\00 - Ens	truct Documents\0.3 -	Analysis\Civil\OSD\DRA	INS\MAINBUIL	DING3					
DRAINS Version:		DRAINS Version 2017.11									
Modeller's Name:		Migueas Moreno	20 00(201)								
Description:		Main Building Area									
DRAINS results prepared from Version 2018.01		Main Bailaing / Tea									
Divality results prepared from version 2010.01											
PIT / NODE DETAILS				Version 8		1				- R	ESULTS
Name	Max HGL	Max Pond	Max Surface	Max Pond	Min	Overflow	Constraint				
i vanc	INIAX FIGE	HGL	Flow Arriving	Volume	Freeboard	(cu.m/s)	Constraint			-	1% AEP
		IIOL	(cu.m/s)	(cu.m)	(m)	(60.111/3)					
PitD1	19.45		0.03	(00.111)	0.58	0	None				
PitB2	19.33		0.009		0.54		None				
PitB1	19.25		0.000		0.24	Ů	None				
PitA1	17.81		0		1.49	0	None				
PitA2	17.55		0		0.13		None				
A3	16.73		0		0.10						
PitH1	20.27		0.012		0.64	0	None			1	
PitB4	19.95		0.008		0.55		Inlet Capacity			1	
PitB3	19.65		0.000		0.55		None				
DP3	22.09		0.004		0.86		None			1	
DP4	21.13		0.005		0.97		None				
PitE4	20.62	21.24	0.016	0.7			Inlet Capacity				
PitE3	20.46		0		0.68		None				
PitE2	20.21		0		0.69		None				
PitE1	19.26		0		1.64		None				
PitG1	19.32		0.007		0.68		None				
PitC1	19.28		0.023		0.14	0	None				
DP5	22.21		0.008		0.74		None				
PITF1	19.28	19.55	0.024	0.3			Inlet Capacity				
LAND1	20.9		0.012		0.35		None				
PitB6	20.1		0.017		0.62	0	None				
PitB5	20.08		0.026		0.57	0.001	Inlet Capacity				
					1	1					
SUB-CATCHMENT DETAILS											
Name	Max	Paved	Grassed	Paved	Grassed	Supp.	Due to Storm				
	Flow Q	Max Q	Max Q	Тс	Тс	Тс	İ İ	Ī			1
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)					
CatD1	0.023	0.023	0	5	5		1% AEP, 5 min				
CatB2	0.007	0.007	0	5	10	5	1% AEP, 5 min	burst, Storm 1			
CatOSD	0.087	0.087	0	5	5	5	1% AEP, 5 min	burst, Storm 1			
CatH1	0.01	0.009	0.001	5	5	5	1% AEP, 5 min	burst, Storm 1			
CatB4	0.005	0.004	0	5	5	5	1% AEP, 5 min	burst, Storm 1			
CatGrass	0.021	0.002	0.02	5	12	5	1% AEP, 15 mi	n burst, Storm	8		
LANDSC-3	0.004	0	0.003	5	10	5	1% AEP, 15 mi	n burst, Storm	5		
LANDSC-4	0.004	0.004	0	5	10		1% AEP, 5 min				
CatE4	0.012	0.011	0.001	5	5	5	1% AEP, 5 min	burst, Storm 1			
CatG1	0.006	0.006	0	5	5		1% AEP, 5 min				
CatC1	0.019	0.019	0	5	5	5	5 1% AEP, 5 min burst, Storm 1				
CatByPass	0.017	0.004	0.012	5	10	5	1% AEP, 10 mi	n burst, Storm	7		

CatB3	0.007	0.007	0	5	5	5	1% AFP 5 m	in burst, Storm	1			·
Cat248200	0.009	0.009	0.001	5	-			in burst, Storm				
CatB6	0.013	0.012	0.001	5	5			in burst, Storm				
CatB5	0.02	0.012	0.001	5	5			in burst, Storm				
	0.02	0.010	0.001						İ İ			
PIPE DETAILS												
Name	Max Q	Max V	Max U/S	Max D/S	Due to Storm							
	(cu.m/s)	(m/s)	HGL (m)	HGL (m)	200 10 010111			1	1			·
D1 TO B2	0.023	1.45	19.362		1% AEP, 5 mi	n burst Storm	1					
B2 TO B1	0.092	1.3	19.267		1% AEP, 10 m							
B1 TO TANK	0.114	1.03	19.222		1% AEP, 10 m							
TANK TO A1	0.051	1.28	18.116		1% AEP, 45 m							
A1 TO A2	0.051	1.28	17.798		1% AEP, 45 m							
A2 TO A3	0.051	1.28	17.43		1% AEP, 20 m							
TO RAINGARDEN	0.025	2.66	16.951	16.729	1% AEP, 45 m	nin burst, Storn	1 9					
H1 TO B5	0.01	1.01	20.218		1% AEP, 5 mi						<u> </u>	
B4 TO B3	0.053	2.3	19.859		1% AEP, 10 m						<u> </u>	
B3 TO B2	0.064	2.97	19.523		1% AEP, 10 m			1	1			
LAND-DP3	0.004	2.02	22.028	19.328	1% AEP, 15 m	nin burst, Storn	1 5					
LAND-DP4	0.004	1.6	21.081		1% AEP, 5 mi							
E4 TO E3	0.016	3.44	20.548	20.463	1% AEP, 10 m	nin burst, Storn	า 1					
E3 TO E2	0.016	2.86	20.4	20.212	1% AEP, 10 m	nin burst, Storn	1 6					
E2 TO E1	0.015	1.17	20.202	19.983	1% AEP, 10 m	nin burst, Storn	า 1					
E1 TO TANK	0.034	0.48	19.284	19.541	1% AEP, 20 m	nin burst, Storn	ו 4					
G1 TO B1	0.006	1.25	19.266	19.229	1% AEP, 5 mi	n burst, Storm	1					
P20540	0.018	0.47	19.236	19.229	1% AEP, 5 mi	n burst, Storm	1					
EX-DP5	0.007	2.4	22.038		1% AEP, 5 mi							
P257158	0.022	0.32	19.26	19.258	1% AEP, 20 m	nin burst, Storn	ו 1					
P285189	0.009	2.29	20.832		1% AEP, 5 mi							
B6 TO B5	0.023	0.79	20.098	20.083	1% AEP, 5 mi	n burst, Storm	1					
B5 TO B4	0.042	1.73	19.993	19.954	1% AEP, 10 m	nin burst, Storn	า 1					
CHANNEL DETAILS												
Name	Max Q	Max V			Due to Storm							
	(cu.m/s)	(m/s)										
OVERFLOW ROUTE DETAILS												
Name	Max Q U/S	Max Q D/S	Safe Q	Max D		Max Width	Max V	Due to Storm				
OF D1 TO B2	0	0	1.38	0	ů	0	0					
OF B2 TO B1	0	•	1.431	0		-					\vdash	
OSD TO STREET	0	0	1.311	0	ů	0	-					
OF A1 TO STREET	0	0	1.479	0	-	0			┥───┤		┟────┤	
OF A2 TO STREET	0	0	1.404	0	0	0	-			4	┟────┤	
OF TO EXISTING SW	0.026	0.026	0.206	0.046		2.33		1% AEP, 30 r	nin burst, Storm	1	┟────┤	
OF H1 TO B5	0	0	1.432	0	0	0	-	10/ 455 / -		4	┟────┤	
OF B4 TO D2	0.001	0.001	1.449	0.008	-	0.84			nin burst, Storm		↓ ↓	
SWALE	0.021	0.021	0.035	0.096	0.05	0.49			nin burst, Storm	ŏ	┟────┤	
OF51353	0	0	1.333	0	0	0	0			7	↓ ↓	
OFByPass	0.017	0.017	1.479	0.027	0.01	4			nin burst, Storm	1	↓ ↓	
OFBYPASS2 OF5167	0	0	1.479	0	0	0	0		├ ───┤		┟────┤	
	0	0	1.48	0	-	-	-		in hungt Otam 1		┟────┤	
OF B5 TO B4	0.001	0.001	1.47	0.009	0	0.94	0.22	1% AEP, 5 m	in burst, Storm 1		├──── ┤	
	1						l	1	↓ ↓		L I	

DETENTION BASIN DETAILS									
Name	Max WL	MaxVol	Max Q	Max Q	Max Q				
			Total	Low Level	High Level				
OSD TANK	19.34	90.8	0.051	0.051	0				
A3 FLOW SPLITTER	17.23	0.4	0.051	0.025	0.026				
Run Log for MAINBUILDING3 run at 18:10:48 on 19/6/2018									
No water upwelling from any pit.									
Freeboard was less than 0.15m at PitA2, PitC1									
Flows were safe in all overflow routes.									

APPENDIX C CIVIL DRAWINGS





TOWER 2, LEVEL 23 DARLING PARK, 201 SUSSEX ST SYDNEY NSW 2000

URBIS.COM.AU Urbis Pty Ltd ABN 50 105 256 228

4 July 2018

Mr Stuart Ardlie Statutory Planner City of Canada Bay Locked Bay 1470 DRUMMOYNE NSW 1470

Via email: stuart.ardlie@canadabay.nsw.gov.au

Dear Stuart,

RE: DA2018/0076 DOMREMY COLLEGE: RESPONSE TO REQUEST FOR ADDITIONAL INFORMATION

We write on behalf of Sydney Catholic Schools (the Applicant) to address the issues raised within your formal request for additional information dated 17 May 2018 and subsequent emails relating to DA2018/0076 for Domremy College, 121 First Avenue, Five Dock. This DA was lodged with the City of Canada Bay Council on 16 March 2018 and sought approval for:

Demolition of two existing building, ancillary structures and removal of select vegetation. Relocation of existing car park and construction of a new two storey building with three temporary demountable buildings to be provided on site during construction.

1. Request for Additional Information

The additional information requested is addressed in **Table 1** and the following documentation:

- Stormwater Management Concept Plan prepared by Enstruct (dated February 2018);
- Revised Site Plan and Shade Structure Section prepared by Hayball Architects (dated 29 June 2018);
- Traffic and Parking Statement prepared by PDC Consultants (dated 3 July 2018);
- Arborist Report prepared by McCardle Aboricultural (dated 28 June 2018).

We note that only limited design changes arise from the response to the RFI, and these changes do not introduce any statutory non-compliances or environmental impacts which differ from the impacts assessed in the Statement of Environmental Effects lodged with the DA.



Table 1 – Response to Request for Information

Requested Information	Response
Stormwater Management	
Hard and electronic copies of the DRAINS Model used are to be provided.	Provided as part of revised Stormwater Management Concept Plan.
Stormwater drainage design calculations shall be provided to justify proposed system components (pits and pipes) sizes and to show flow rate through proposed discharge pipe system.	The DRAINS model contains design calculations of proposed stormwater system components and flow rates.
A plan layout of proposed OSD system is required and shall show its dimensions, size and location of access points, surface levels, invert levels, etc.	Refer to DWG CV-0211, STORMWATER DETAILS SHEET 1
Cross sectional details of required OSD shall also be provided.	Refer to DWG CV-0211, STORMWATER DETAILS SHEET 1
Access requirements for OSD must not be more than 5m apart.	Refer to DWG CV-0211, STORMWATER DETAILS SHEET 1
In accordance with Council's current DCP – Appendix 2 "Engineering Specifications", a maximum 50% rainwater re-use volume is permitted to be deducted from On-site Detention (OSD) system based on BASIX requirements.	
As per Council's current DCP – Appendix 2 Engineering specifications, Rainwater Re-use system with a minimum capacity of 5000 Litres shall be provided.	Email correspondence from Council dated 19 June 2018 confirms these
Cross sectional details of required rainwater tank shall be provided.	requirements do not apply to the DA.
Should downpipes be charged to rainwater re-use tank, clean out pits/inspection eyes shall be installed and located at the lowest point of charged lines. The locations shall be clearly marked on the plan. A section through clean out pit shall be provided.	
The consultant shall demonstrate that OSD will not have "Drowned outlet". A drowned outlet occurs when the water level at the connection point "Kerb Inlet Pit" is higher than the orifice centreline level. The tail- water influences will affect the discharge rate. Therefore, Hydraulic Grade Line assessment of the proposed discharge system shall be undertaken from the existing Kerb Inlet Pit to demonstrate that the Drowned Outlet does not occur at the OSDs. If the HGL levels at the point of connection are not known, HGL can be determined from the level which is 150mm below the surface level of the discharge pit.	Refer to DWG CV-0512, SITEWORKS DETAILS SHEET 2



Requested Information	Response
High Early Discharge (HED) shall also be provided to allow minor flow to bypass the storage facility and to prevent frequent maintenance of required OSD. Majority of the inlet pipes shall be directly connected to a Discharge Control Pit to prevent main storage being utilised all the time. If no (HED) is provided, basic storage volume shall be increased by 20%.	Refer to DWG CV-0211, STORMWATER DETAILS SHEET 1
A boundary discharge pit shall be provided and a section through it shall also be provided showing a silt and gross pollutant trap being included in accordance with Council' current Development Control Plan, Appendix 2 - Engineering specifications along with inlet and outlet connections etc.	Refer to DWG CV-0202, STORMWATER PLAN SHEET 2 and DWG CV-0212, STORMWATER DETAILS SHEET 2
Calculations to determine the size of discharge control device such as orifice plate shall be provided.	Refer to Revised Stormwater Concept Plan Section 6.1
Sediment and Erosion control measures and proposed discharge from sediment basins shall be incorporated in the Stormwater Concept Plan	Refer to DWG CV-0202 & CV-0400
Driveway Access	
Longitudinal section along the extreme wheel path of proposed driveway in First Avenue. The section shall extend from the centre line of the roadway and shall include all gradients including footpath cross fall to be at a maximum of 2.5%, change of grade and grade transition details and levels. It shall also include a standard layback crossing with a maximum of 100mm level difference from the invert of the gutter to top of layback. Layback levels shall be consistent with the detail survey levels.	Refer to DWG CV-0512 DRIVEWAY SECTION and Traffic Statement
The driveway profile shall also demonstrate compliance with the scraping provisions of AS/NZS 2890.1:2004 based on the 85th percentile vehicles ground clearance templates.	Refer Traffic Statement
Driveway entrance shall be perpendicular to the kerb and gutter alignment and should not be designed with kerb returns.	Refer to DWG CV-0512 DRIVEWAY PLAN and Traffic Statement
All redundant driveways shall be removed and footway and footpath reinstated. Any redundant stormwater outlets shall also be removed.	Refer to DWG CV-0550 PAVEMENT PLAN and Traffic Statement
Tree Officer and Heritage Advisor	
Tree No. 38 (<i>Phoenix Canariensis</i>) is to be retained. As such the driveway design and layout will need to be amended to both retain this tree and ensure the ongoing longevity is not impacted by the driveway location and construction. Please amend the proposal and provide a supporting statement from both your traffic engineer and your arborist proposing suitable tree protection measures.	As outlined in the Revised Site Plan and Traffic Statement, the alignment of the First Avenue driveway and internal roadway have been reconfigured to ensure that these are clear of Tree 38 and importantly, that Tree 38 is able to be retained.



Requested Information	Response
	In addition, the following tree protection measures to minimise impacts to the tree are outlined in Appendix D of the revised Arborist Report:
	- Tree protection fencing;
	- Trunk and branch protection with boards and padding strapped to trees;
	- Ground protection measures including a permeable membrane or crushed rock below rumble boards.

2. Request for Additional Information

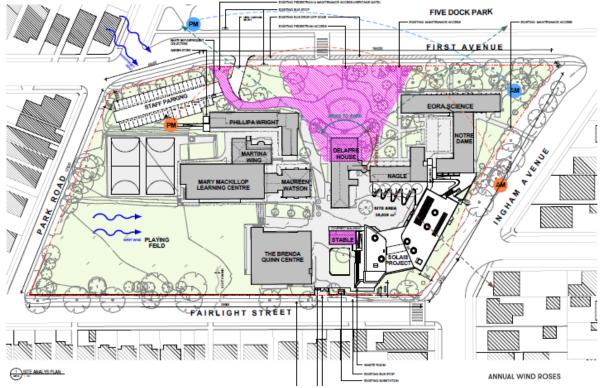
Since lodgement of the DA with Council, the Applicant has amended the proposal to include a new shade structure to the north of the Mary Mackillop Learning Centre. Pursuant to section 55(1) of the *Environmental Planning and Assessment Regulation 2000*, this letter formally requests to amend the DA to seek development consent for the construction of the shade structure.

The proposed structure will be freestanding on steel posts and measure 22m by 13m, as shown in the revised Site Plan and Shade Structure Section. The structure will have a maximum height of 7.1m to match the eaves of the neighbouring Mary Mackillop Learning Centre. The existing grassed area below the shade structure will be replaced with a new paved surface or soft-fall.

Given the location of the shade structure towards the centre of the site, views of the structure from residential properties surrounding the site will be limited. In addition, the structure will not impact on the heritage values or setting of the identified heritage items within the site (refer **Figure 1**), given it is screened by surrounding buildings, including the Phillip Wright Building and Mary Mackillop Learning Centre.



Figure 1 – Location of Heritage Items (shown in Pink)



Source: Hayball and Urbis

In light of the above, the inclusion of the shade structure as part of the proposal is considered acceptable.

3. Summary

We trust the additional documentation will assist in your continued assessment of the development application. The proposal represents a sound development outcome worthy of Council support and ultimately approval from the Sydney Eastern City Planning Panel.

Should you require anything further please contact me on 8233 7668 or edethridge@urbis.com.au.

Yours sincerely,

Detedge

Erin Dethridge Senior Consultant

License No. TCAA13/1042/14 Jim McArdle Climbing Consulting Arborist

Arborist Impact Assessment



Sydney Catholic Education Office Domremy College, 121 First Avenue, Five Dock, New South Wales 28th of June 2018

CONSULTING ARBORIST

Jim McArdle B.Ed (Science) Dip.Arb L5

0449 228 788 jim@mcardlearborist.com.au





Member 13104214

Tel: 02 9651 7880	PO Box 608 Round Corner Dural NSW 2158	www.mcardlearborist.com.au
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McArdle Arboricultural Consultancy Pty Ltd

TABLE OF CONTENTS

SECTION I		
TABLE OF CONT	ENTS	2
1.0 ABSTRACT		3
2.0 INTRODUCT	ION	4
3.0 REFERENCES	S	4
4.0 METHODOL	OGY	5
5.0 SITE		6
6.0 TREE SURVE	Y TABLE 1	7
7.0 ANALYSIS O	F MAPPING CONTROLS	15
8.0 DISCUSSION	1	17
9.0 HOLDING PO	DINT	19
10.0 RECOMME	INDATION	20
11.0 GLOSSARY		21
12.0 BIBLIOGRA	\PHY	22
WEBSITE		22
SECTION II		
APPENDIX A	TULE – TREE USEFUL LIFE EXPECTANCY	23
APPENDIX B	HEALTH & STRUCTURAL CONDITION OF TREE- Visual	24
APPENDIX C	RETENTION VALUES	25
APPENDIX D	TREE PROTECTION	26
PROHIBITIONS		27
APPENDIX E	TREE PLANTING SPECIFICATIONS AND MAINTENANCE	28
APPENDIX F	INDIGENOUS TREE REPLENISHMENT	29
DISCLAIMER		30
SECTION III		
TREE IMPACTS I	PLANS	32

TREE MANAGEMENT PLAN33UPDATED DRIVEWAY SECTION34UPDATED PLAN35FINAL PROPOSED SITE PLAN36

Arborist Impact Assessment and Tree Management Plan 1.0 ABSTRACT

1.1 The Catholic Education Office has commissioned an Arborist Impact Report relating to one hundred and seven (117) trees at Domremy College, First Avenue, Five Dock, New South Wales. Of these trees, (6) six will be removed and (15) fifteen will have encroachments to their TPZ. Ten of these trees are encroached by less than 10% are adjacent the carpark aligned to First Avenue. No trees of high value will be impacted, however (2) two moderate retention value trees may be impacted up to ten percent and greater by the newly installed street access from First Avenue.

1.2 The planning controls state that the site has heritage items of the old convent and planted trees have suitable values. The six (6) trees removed of low retention value will be replenished with indigenous species suitable for a school environment. Holding points include Tree Protection Fencing and certification of the replenishment.

1.3 The methodology used include Visual Tree Assessment (VTA) and Impact Assessment utilizing AS4970-200 Protection of Trees on Development site.

Arborist Impact Assessment and Tree Management Plan 2.0 INTRODUCTION

2.1 The Catholic Education Office commissioned an Arborist Impact Report relating to one hundred and seven (107) trees at Domremy College, First Avenue, Five Dock, New South Wales. (6) Six trees of low to moderate value will be removed and replenished according to the Tree management plan. Indigenous tree stock of 40 litre potted volume, including <u>Lophostemon</u> <u>confertus</u> (Brush Box) and <u>Elaeocarpus reticulatus</u> (Blueberry Ash) or <u>Callistemon viminalis</u> (Red Bottle Brush)would be preferred to ensure character of the sited area for perpetuity and biodiversity values are maintained.

2.2(15) Fifteen trees will be impacted within there TPZ-Tree Protection Zone, but are retainable with supervisory AQF Level 5 supervision, certification and protection of these trees. Installing a new access drive and carpark will necessitate the encroachments and rootmapping with root pruning and pruning according to As4373 2007 Pruning of Amenity Trees, would be recommended by an AQF Level 5 arborist for these trees.

2.32 McArdle Arboricultural Consultancy Pty Ltd prepared the report. The arboricultural impact report is developed to assess the trees at the above address for health and status. James McArdle, AQF level 5 Consulting Arborist conducted the evaluation using Visual Tree Assessment (VTA) method for biological and lower level mechanical functions on the 4th of March 2017 and reviewed on the 28th June 2018. The systems are in accordance with industry best practice and impact assessments are based upon the Australian Standards, Protection of Trees on Development sites AS4970-2009.

3.0 REFERENCES

1. Canada Bay Local Environmental Plan 2013.

2. Canada Bay Development Control Plan 2013.

3. Site Plan of Details and Levels over Lot 1 in DP128043 known as No121 First Avenue 'Domremy College". LTS-Lockley Registered Surveyors. September 2016. Sheets 1-13.

4. Proposed Site Plan Author Hayball Architects Dated 28/6/18 DWG DA01.02 V6.

Arborist Impact Assessment and Tree Management Plan 4.0 METHODOLOGY

4.1 A tree assessment uses a ground Visual Tree Assessment (VTA) method employed in this report. The VTA system is based on the theory of tree biology, physiology and tree architecture and structure and is a method used to identify visible signs on trees that indicate health and potential hazards. It identifies low level mechanical functions and biological functions according to Mattheck and Breloer (1994).

4.2 The collection of data is performed in the field by an Environmental Scientist, AQF Level 5 arborist. The assessment summaries the species, height and diameter, the tree health and structural condition of the tree, hazards, and retention categories were assigned. The scale drawing ratio were absent from the 'Arborist brief' and impacts percentages have not been calculated. These could be supplied on production of scaled drawings on the construction brief.

4.3 This data was recorded in a Tree Survey Table and various assessment methods were used including:

1. Tree Useful Life Expectancy. Adapted from Jeremy Barrel (SULE) gives extra assessment life expectancy categories range to no potential for life expectancy. Appendix A.

2. Health & Structural Condition of Tree Assessment. This describes the vigour and vitality of the tree. This has conditions associated with the VTA found in Appendix B.

3. Retention Values according to Melanie Howden and TCAA significance values. Appendix C.

4.Impacts are based on AS4970 2009 Protection of Trees on Development Sites. Extract in appendix D and setbacks given in table 1.

5.1 The site at Domremy College, First Avenue, Five Dock, New South Wales.

5.2 The collection of survey data was limited and an inspection was conducted on the 4th of March 2017 and reviewed on 28th June 2018.

SCALED SITE MAP



Plate 1. Aerial Plate of the site. Courtesy of Google maps.¹

¹ (https://www.google.com.au/maps/)

Tree No.	Locality	Scientific& Common Name	Crown Spread m	Height (m)	Diam (cm)	TPZ SRZ (m)	Condition of Tree & Failure potential (Health & Structure-defects & measurements)	TULE	Retention Value	Impacts or Works
1.	Car park	<u>Cinnamomum camphora</u> Camphor laurel	20	9	132 133	15 3.73	Mature, good condition but poor development, stub cut at north side.	2a	Mod-high	Impact to TPZ ground protection and sensitive construction measure.
2.		<u>Cinnamomum camphora</u> Camphor laurel	W10 e10	7	60 80	7.2 3.01	Mature, lean to the west, suppressed.	2d	Mod	RETAIN
3.		<u>Cinnamomum camphora</u> Camphor laurel	N2 E5 W5 S5	9	100 104	12 3.36	Mature, inclusion at 1.4m, two main stems.	3d	Mod	RETAIN
4.		<u>Pittosporum undulatum</u> Sweet pittosporum	6	5.5	32 36	3.84 2.15	Mature, cavity at 1m	2d	Mod	RETAIN
5.		<u>Cinnamomum camphora</u> Camphor laurel	9	10	125 127	15 3.66	Mature, root damage and swelling, heavily pruned at 1.5m (300mm cut).	2d	Mod-high	RETAIN
6.		<u>Lophostemon confertus</u> Brush box	4	5	24 29	2.88 1.97	Immature, excellent condition	2a	Mod	RETAIN
7.		<u>Eucalyptus paniculata</u> Grey gum	4	5	34 34	4.08 2.1	Mature, good condition but poor development.	2a	Mod	RETAIN
8.		<u>Leptospermum Sp.</u> Tea tree	4	6	30 34	3.6 2.1	Mature, some dehydration damage, stem failed at 1m (200mm).	2d	Low-Mod	RETAIN
9.		<u>Leptospermum Sp.</u> Tea tree	3	4	12 15	2 1.5	Mature, heavily pruned at 1m, lean to the east.	3d	Low	RETAIN
10.		<u>Leptospermum Sp.</u> Tea tree	4	6	16 18	2 1.61	Mature, good condition but poor development, lean to the east.	3d	Low	RETAIN
11.		<u>Cinnamomum camphora</u> Camphor laurel	8	8	30/56 95	7.68 0.95	Mature, two stems, minor dehydration.	2d	Mod	RETAIN
12.		<u>Leptospermum Sp.</u> Tea tree	3	6	15 20	2 1.68	Mature, lean west.	2d	Low	RETAIN
13		<u>Leptospermum Sp.</u> Tea tree	5	6	12/20/ 14 30	3.24 2	Mature, sparse foliage crown, inclusion at base.	3d	Low-Mod	RETAIN
14		<u>Cinnamomum camphora</u> Camphor laurel	8	8	37/40 82	6.48 3.04	Mature, unbalanced canopy, slight lean west, two main stems	3d	Low-Mod	RETAIN
15		<u>Leptospermum Sp.</u> Tea tree	3	6	25 34	3 2.1	Immature, stem cut at base (90mm), lean.	3d	low	RETAIN

Arborist Impact Assessment and Tree Management Plan

Tree No.	Locality	Scientific& Common Name	Crown Spread m	Height (m)	Diam (cm)	TPZ SRZ (m)	Condition of Tree & Failure potential (Health &Structure-defects & measurements)	TULE	Retention Value	Impacts or Works
16		<u>Leptospermum Sp.</u> Tea tree	5	6	20/15/ 12/14 35	3.72 2.13	Mature, inclusion, sparse foliage crown, dieback at 20%.	3d	Low-Mod	RETAIN
17		<u>Leptospermum Sp.</u> Tea tree	4	5	15 18	2 1.61	Immature, heavily pruned at base, sparse foliage crown.	3d	Low	RETAIN
18		<u>Cinnamomum camphora</u> Camphor laurel	9	8	30/34 36/43	5.4 2.45	Mature, good condition but poor development.	2d	Mod	RETAIN
19	West, fence near sewage	<u>Leptospermum Sp.</u> Tea tree	7	7	23/30/ 20/10/ 10 55	5.4 2.57	Mature, heavily pruned at 1.3m, sparse foliage crown	3d	Low- Mod	RETAIN
20		<u>Lophostemon confertus</u> Brush box	4	6	25 28	3 1.94	Immature, twin leader, buildup of mulch at base near concrete pylon.	2a	Low	RETAIN
21		<u>Lophostemon confertus</u> Brush box	4	6	25 28	3 1.94	Immature, excellent condition.	2a	Low- Mod	RETAIN
22		<u>Leptospermum Sp.</u> Tea tree	5	7	23/37 67	5.28 2.8	Mature, unbalanced canopy and lean west, stem cut 350mm at 50cm, minor fungal attack.	3d	Low- Mod	RETAIN
23	West fence	<u>Ulmus parvifolia</u> Chinese elm	3	4	12 15	2 1.5	Immature, excellent condition	la	Low	RETAIN
24		<u>Eucalyptus paniculata</u> Grey gum	6	10	26 16	3.12 1.53	Immature, good condition but poor development, some borer damage.	2d	Low- Mod	RETAIN
25		<u>Eucalyptus saligna</u> Blue box	8	9	30 35	3.6 2.13	Immature, some borer damage, unbalanced canopy east.	2d	Low- Mod	RETAIN
26		<u>Eucalyptus saligna</u> Blue box	4	8	18 22	2.16 1.75	Immature, some borer damage.	2d	Mod	RETAIN
27		<u>Eucalyptus paniculata</u> Large fruited ironbark	7	12	45 50	5.4 2.47	Immature, some insect damage on branch.	2d	Mod	RETAIN
28		<u>Eucalyptus paniculata</u> Grey ironbark	5	10	33 36	3.96 2.15	Immature, good condition but poor development, inclusion at 4m, sparse foliage crown.	2d	Mod	RETAIN
29		<u>Eucalyptus saligna</u> Blue box	s-w3 e-w6	13	20/15 47	3 2.41	Immature, physical damage- broken branch, unbalanced canopy north west.	2d	Mod-high	RETAIN
30		<u>Eucalyptus saligna</u> Blue box	7 east	12	47/49 84	8.16 3.08	Immature, unbalance canopy to the east.	2d	Mod	RETAIN

Arborist Impact Assessment and Tree Management Plan

Tree No.	Locality	Scientific& Common Name	Crown Spread m	Height (m)	Diam (cm)	TPZ SRZ (m)	Condition of Tree & Failure potential (Health & Structure-defects & measurements)	TULE	Retention Value	Impacts or Works
31		<u>Eucalyptus tereticornis</u> Forest red gum	8	12	50 53	6 2.53	Immature, good condition but poor development	2a	Mod	Adjacent proposed carpark. Ground and trunk protection.
32		<u>Lophostemon confertus</u> Brush box	8	10	45/22/ 15/30/ 30 77	8.04 2.97	Mature, Immature, good condition but poor development.	2a	Mod	Adjacent proposed carpark. Ground and trunk protection
33		<u>Corymbia maculata</u> Spotted gum	5	12	35 45	4.2 2.37	Immature, excellent condition.	2a	Mod	Adjacent proposed carpark Ground and trunk protection
34		<u>Corymbia maculata</u> Spotted gum	7	12	33 37	3.96 2.18	Immature, excellent condition	2a	Mod	Adjacent proposed carpark Ground and trunk protection
35		<u>Corymbia maculata</u> Spotted gum	5	10	25 27	3 1.91	Immature, excellent condition, compacted around base.	2a	Mod	Adjacent proposed carpark. Ground and trunk protection
36		<u>Lophostemon confertus</u> Brush box	7	10	27/28/ 38/18 79	6.84 3	Mature, slight lean to the north west.	2a	Mod	Adjacent proposed carpark Ground and trunk protection
37	Adjacent gate	<u>Phoenix canariensis</u> Phoenix palm	6	8	58 55	6.96 2.57	Mature, good condition but poor development.	2a	Mod-high	Retain. Adjacent proposed carpark Ground and trunk protection
38	Adjacent gate	<u>Phoenix canariensis</u> Phoenix palm	6	9	60 66	7.2 2.78	Mature, good condition but poor development	2a	Mod-high	Retain. Adjacent proposed carpark Ground and trunk protection
39		<u>Callistemon viminalis</u> Bottle brush	4	3	10*4 20	4.8 1.68	Immature, excellent condition, small shrub.	2a	Low- Mod	Remove impacted by New Building. Replenish tree.
40		<u>Brachychiton acerifolius</u> Flame tree	5	7	24/22 27	3.96 1.91	Immature, inclusion at 1m.	2a	Low- Mod	Remove impacted by New Building. Replenish tree.
41		<u>Melaleuca Sp.</u> Paperbark	5	5	20/26/ 25 63	4.92 2.73	Immature, inclusion at base, lean to the west.	2d	Low	Adjacent proposed carpark Ground and trunk protection
42		<u>Phoenix canariensis</u> Phoenix palm	6	5	60 70	7.2 2.85	Mature, slight lean to the west.	2d	Mod-high	RETAIN
43		<u>Lophostemon confertus</u> brush box	5	7	37/42/ 32 92	7.68 3.2	Mature, some physical damage, heavily pruned, unbalanced canopy, 350mm cut at 1m west side.	2a	Mod	RETAIN
44	North fence	<u>Pinus radiata</u> Radiata pine	9	11	70 75	8.4 2.93	Mature, previously pruned.	2d	Mod	Impacted by 10% &greater but remains viable. AQF supervision. RETAIN.
45	Adjacent drive way	<u>Phoenix canariensis</u> Phoenix palm	5	7	60 65	7.2 2.76	Immature, good condition but poor development	2a	Mod	Impacted by 10%&greater but remains viable. AQF supervision RETAIN.

Arborist Impact Assessment and Tree Management Plan

Tree No.	Locality	Scientific& Common Name	Crown Spread m	Height (m)	Diam (cm)	TPZ SRZ (m)	Condition of Tree (Health & Structure-defects)	TULE	Retention Value	Impacts or Works
46		<u>Cinnamomum camphora</u> Camphor laurel	10	7	40/40/ 37 102	8.16 3.34	Mature, unbalanced canopy, previously pruned,	3d	Low- Mod	RETAIN
47		<u>Ornamental Sp.</u>	e-w 12 n-s 5	3	30/25/ 25/15	5.88	Mature, cavity at 1.5m west.	3d	Low- Mod	RETAIN
48		<u>Gleditsia tricanthos</u> Honey locust	7	6	22/22/ 22	4.56	Mature, unbalanced canopy, some physical damage (250mm)	2a	Low- Mod	RETAIN
49		<u>Phoenix canariensis</u> Phoenix palm	6	8	75 82	9 3.04	Mature, excellent condition.	2a	Mod-high	RETAIN
50		<u>Tibouchina Sp.</u>	3	5	20 28	2.4 1.94	Immature, some physical damage, lean and unbalanced canopy east.	2d	Low- Mod	RETAIN
51		<u>Tibouchina Sp.</u>	3	5	28/22/ 14 56	4.56 2.59	Immature, twin stem.	2a	Mod	RETAIN
52		<u>Phoenix canariensis</u> Phoenix palm	6	9	22	2.64	Mature, physical damage due to barrier south.	2d	-	RETAIN
53	Adjacent path	<u>Eucalyptus microcorys</u> Tallow wood	3	6	23 28	2.76 1.94	Immature, good condition but poor development.	2a	Low	RETAIN
54		<u>Xmas bush Sp.</u>	4	5	20 18	2.4 1.61	Immature, good condition but poor development,	2a	Low	RETAIN
55	Seating area	<u>Camellia japonica</u> Japanese camellia	6	5	40 41	4.8 2.28	Immature, good condition but poor development	2a	Low- Mod	RETAIN
56		<u>Syncarpia glomulifera</u> Turpentine	5	6	26 26	3.12 1.88	Immature, excellent condition.	2a	Low- Mod	RETAIN
57	Garden bed	<u>Cupaniopsis</u> <u>anacardioides</u> Tuckeroo	4	5	22 27	2.64 1.91	Immature, good condition but poor development, physical damage at 4m (tarpaulin)	2a	Low	RETAIN
58		<u>Phoenix canariensis</u> Phoenix palm	6	7.5	70 50	8.4 2.47	Mature, excellent condition.	2a	Mod	RETAIN
59		<u>Phoenix canariensis</u> Phoenix palm	6	7	66 78	7.92 2.98	Mature, excellent condition.	2a	Mod	RETAIN
60		<u>Eucalyptus paniculata</u> Grey ironbark	5	10	32 36	3.84 2.15	Immature, good condition but poor development	2a	Mod	RETAIN
61		<u>Ornamental Sp.</u>	5	3	20/15/ 12/12/ 8 40	3.72 2.25	mature, good condition but poor development	2a	Low- Mod	RETAIN

Arborist Impact Assessment and Tree Management Plan

Tree No.	Locality	Scientific& Common Name	Crown Spread m	Height (m)	Diam (cm)	TPZ SRZ (m)	Condition of Tree (Health &Structure-defects)	TULE	Retention Value	Impacts or Works
62		<u>Pinus radiata</u> Radiata pine	5	7.5	54 56	6.48 2,59	Immature, some root damage, lean to the west.	2a	Low	RETAIN
63		<u>Cinnamomum camphora</u> Camphor laurel	8	8	37/34/ 40 124	7.68 3.62	Mature, plants growing in cavity at 1m, previously cut.	2d	Mod	RETAIN
64		<u>Camellia japonica</u> Japanese camellia	3	4	10*7	8.4	Immature, good condition but poor development, unbalanced canopy.	2a	Low	RETAIN
65	Front fence	<u>Camellia japonica</u> Japanese camellia	3	3	15*9 70	15 2.85	Immature, excellent condition.	2a	Low	RETAIN
66		<u>Camellia japonica</u> Japanese camellia	3	3	3*10 30	3.6 2	Immature, good condition but poor development, dead branch at 50cm (150mm).	2a	Low	RETAIN
67		<u>Callistemon viminalis</u> Bottle brush	8	7	16/20/ 20/20 57	4.56 2.61	Mature, cavity at 1m east.	3d	Mod	Minor pruning to canopy and tree protection. RETAIN.
68		<u>Callistemon viminalis</u> Bottle brush	5	6	20/25 32	3.84 2.05	Mature, lean and unbalanced canopy to the south, suppressed.	3d	Low- Mod	Minor pruning to canopy and tree protection. RETAIN.
69		<u>Syzygium smithii</u> Lilly pilly	3	7	14 15	2 1.5	Immature, lean west.	2a	Low	RETAIN
70	Adjacent parking	<i>Jacaranda mimosifolia</i> Jacaranda	6	8	30/26 45	4.8 2.37	Immature, two main stems.	2d	Mod	Remove impacted by New Building. Replenish tree.
71		<u>Brachychiton acerifolius</u> Flame tree	4	7	52 55	6.24 2.57	Mature, heavily pruned at 4m (300mm cut)	3d	Mod	Remove impacted by New Building. Replenish tree.
72		<u>Lophostemon confertus</u> Brush box	8	11	87 89	10.44 3.15	Mature, good condition but poor development, minor dehydration.	2d	Mod-high	Remove impacted by New Building. Replenish tree.
73		<u>Lophostemon confertus</u> Brush box	7	8	45/48 78	7.92 2.98	Mature, lean to the west heavily pruned at 4m. Surrounding roots under asphalt.	2a	Mod	Remove impacted by New Building. Replenish tree.
74		<u>Callistemon viminalis</u> Bottlebrush	4	5	10/10/ 10 20	2.04 1.68	Immature, good condition but poor development	2a	Low	RETAIN
75		<u>Banksia integrifolia</u> Coastal banksia	3	5	12/12 20	2.04 1.68	Immature, unbalanced canopy west	2d	Low	RETAIN
76		<u>Melaleuca quinquenervia</u> Narrow leaf paper bark	2	5	14 15	2 1.5	Immature, excellent condition	2a	Low	RETAIN
77		<u>Tristaniopsis laurina</u> Water gum	3	5	14 15	2 1.5	Immature, excellent condition	2a	Low	RETAIN

Arborist Impact Assessment and Tree Management Plan

Tree No.	Locality	Scientific& Common Name	Crown Spread m	Height (m)	Diam (cm)	TPZ SRZ (m)	Condition of Tree (Health & Structure-defects)	TULE	Retention Value	Impacts or Works
78	North side	<u>Dead Pittosporum sp.</u>	-	7	30 40	3.6 2.25	Dead tree	4c	Very low	Remove
79	Fence	<u>Cuppressus sp.</u> <u>Pine</u>	14	18	109 120	13.08 3.57	Mature, heavily pruned at 3 and 3.5m (300mm), lean and unbalanced canopy south east.	3d	Mod-high	RETAIN
80		<u>Pittosporum undulatum</u> Sweet pittosporum	5	7	22 25	2.64 1.85	Immature, unbalanced canopy and lean west.	2a	Mod	RETAIN
81	Front	<u>Cinnamomum camphora</u> Camphor laurel	7	10	85 85	10.2 3.09	mature, good condition but poor development, twin stem.	2d	Mod	RETAIN
82		<u>Cinnamomum camphora</u> Camphor laurel	8	8	46/43/ 34 134	8.64 3.27	Mature, some root damage east side, dehydration.	2d	Mod	RETAIN
83		<u>Cinnamomum camphora</u> Camphor laurel	11	7	26/25/ 40 66	6 2.78	Mature, sparse foliage crown, previously pruned, broken branch.	3d	Low	RETAIN
84		<u>Ornamental sp.</u>	4	4	30 40	3.6 2.25	Immature, multi stemmed.	2d	Very low	RETAIN
85		<u>Cinnamomum camphora</u> Camphor laurel	4	7	10*8 45	9.6 2.37	Multi stemmed	2d	Low	RETAIN
86		<u>Pittosporum undulatum</u> Sweet pittosporum	4	5	10/15 26	2.16 1.88	Immature, unbalanced canopy and lean west	3d	Low	RETAIN
87		<u>Cinnamomum camphora</u> Camphor laurel	10	10	41/33/ 33 113	7.44 3.48	Mature, cavity at 1m, heavily pruned.	3d	Low- Mod	RETAIN
88		<u>Pittosporum undulatum</u> Sweet pittosporum	5	7	22/16/ 18/16 40	4.32 2.25	Mature, root damage and cavity at roots north side.	3d	-	RETAIN
89		<u>Cinnamomum camphora</u> Camphor laurel	7	7	13/30/ 30 70	5.28 2.85	Immature, dieback is greater than 20%, sparse foliage crown.	3a	Mod	RETAIN
90		<u>Cinnamomum camphora</u> Camphor laurel	8	7	38/32/ 32	7.08	Mature, cavity at 1m, sparse foliage crown, girdling root, previously pruned.	3a	Mod	RETAIN
91	North fence	<u>Cinnamomum camphora</u> Camphor laurel	5	6	18/12/ 20 36	3.48 2.05	Immature, some epicormics, sparse foliage crown.	3d	Low	RETAIN
92	North fence	<u>Pittosporum undulatum</u> Sweet pittosporum	5	5	15/14/ 21	3.48	Mature, three main stems, some dehydration.	3d	Low	RETAIN

Arborist Impact Assessment and Tree Management Plan

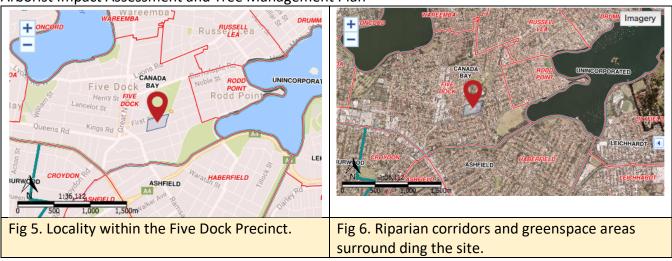
Tree No.	Locality	Scientific& Common Name	Crown Spread m	Height (m)	Diam (cm)	TPZ SRZ (m)	Condition of Tree (Health &Structure-defects)	TULE	Retention Value	Impacts or Works
93		<u>Cuppressus sempervirens</u> Mediterranean cypress	6	12	149 149	15 3.91	Mature, heavily pruned at base to 3m, spreading habit.	3d	Mod-high	RETAIN
94		<u>Cinnamomum camphora</u> Camphor laurel	12	8	80*9 149	15 3.91	Mature, nine stems	-	Mod	RETAIN
95		<u>Corymbia maculata</u> Spotted gum	14	18	120 124	14.4 3.62	Some fungal damage at base	2d	High	RETAIN
96		<u>Cinnamomum camphora</u> Camphor laurel	10	10	50/40/ 30 80	8.52 3.01	Over mature, cavity on east side, cavity west at 2m	4c	Very low	Remove
97	X4	<u>Camellia sasanqua</u> Sasanqua camellia	3	3-4	10*3 20	3.6 1.68	Immature, excellent condition	2a	Low	RETAIN
98		<u>Lagerstroemia</u> Crepe myrtle	3	5	10*7 25	8.4 1.85	Immature, good condition but poor development, heavily pruned at 4m.	3a	Low	RETAIN
99	Adjacent building	<u>Ulmus parvifolia</u> Chinese elm	5	3	14 15	2 1.5	Immature, excellent condition	1a	Low	RETAIN
100	Street scape east side	<u>Lophostemon confertus</u> Brush box	8	7	36 45	4.32 2.37	Immature, good condition but poor development	2a	Mod	RETAIN
101	Street scape east side	<u>Cinnamomum camphora</u> Camphor laurel	10	10	60/30/ 38	9.24	Over mature, cavity at base (60cm depth)	4a	Low	RETAIN
102	Street scape east side	<u>Lophostemon confertus</u> Brush box	10	8	80/25/ 26 78	10.56 2.98	Mature, cavity at 4m and dehydration	3d	Mod	RETAIN
103	Street scape east side	<u>Pinus radiata</u> Radiata pine	15	17	96 101	11.52 3.32	Mature, unbalanced canopy and lean to the west, some termite damage.	3d	Mod-high	Impact to TPZ .requires ground and Trunk Protection. RETAIN
104		<u>Pinus ayacahuite</u> Mexican pine	14	18	41 41	4.92 2.28	mature, good condition but poor development, slight lean northwest.	2d	High	RETAIN
105		<u>Cinnamomum camphora</u> Camphor laurel	W10 E4 N4 S0	8	45 48	5.4 2.43	Mature, cavity at base (30cm), heavy lean north.	2d	Low- Mod	RETAIN
106		<u>Cinnamomum camphora</u> Camphor laurel	12	12	54 58	6.48 2.63	Mature, unbalanced canopy east, minor pruning.	2d	Mod	RETAIN
107		<u>Cinnamomum camphora</u> Camphor laurel	10 to the east	13	60 70	7.2 2.85	Mature, unbalanced canopy east.	2d	Mod	RETAIN
108		<u>Pinus ayacahuite</u> Mexican pine	16	18	110 108	13.2 3.42	Mature, two main stems, good condition but poor development, minor fungal attack.	2a	High	RETAIN

Arborist Impact Assessment and Tree Management Plan

Tree No.	Locality	Scientific& Common Name	Crown Spread	Height (m)	Diam (cm)	TPZ SRZ	Condition of Tree (Health & Structure-defects)	TULE	Retention Value	Impacts or Works
			m			(m)				
109		<u>Cinnamomum camphora</u> Camphor laurel	8	8	42/26/ 31/18/ 10 98	7.44 3.28	Mature, multi-stemmed.and has a spreading habit.	2a	Low-	RETAIN
110		<u>Cinnamomum camphora</u> Camphor laurel	18	12	106 103	12.72 3.35	Mature, good condition but poor development, unbalanced canopy east	2a	Mod-high	RETAIN
111	Street scape	<u>Cinnamomum camphora</u> Camphor laurel	6	8	53 55	6.36 2.57	Immature, unbalanced canopy south, heavily pruned at 2m (350mm cut)	3d	Low- Mod	RETAIN
112	South side	<u>Cinnamomum camphora</u> Camphor laurel	8	9	84 89	10.08 3.15	Mature, dehydration.	2a	Mod	RETAIN
113	South side	<u>Lophostemon confertus</u> Brush box	8	12	65 70	7.8 2.85	Mature, previously pruned, good condition but poor development.	2a	Mod-high	RETAIN
114		<u>Lophostemon confertus</u> Brush box	10	10	66 70	7.92 2.85	Mature, old, heavily pruned (callous), minor dehydration.	2e	Mod	RETAIN
115		<u>Ficus rubiginosa</u> Port Jackson fig	11	10	55 58	6.6 2.63	Immature, very unusually pruned, with crown lifting and adjacent pole. Canopy is a broad dome	2d	Mod	RETAIN
116		<u>Cinnamomum camphora</u> Camphor laurel	10	10	77 80	9.24 3.01	Semi mature, cut stem at 3m (350mm), some dehydration	3d	Mod-high	RETAIN
117		<u>Cinnamomum camphora</u> Camphor laurel	12	11	93 98	11.16 3.28	Semi mature, sparse foliage crown and minor decay.	3d	Mod	RETAIN

7.0 ANALYSIS OF MAPPING CONTROLS

Canada Bay Local Environmental Plan 2013 Following are mapping sets that detail each mapping theme, http://www.legislation.nsw.gov.au; https://maps.planningportal.nsw.gov.au/ **Planning Portal Map** Land Zoning + R2 - Low Density Residential : (pub. 2013-08-02) R2 + RE1 - Public Recreation : (pub. 2013-08-02) 1-4 514 Fig 2. Land Zoning R2 Low Density Residential. Fig 1. Zoning is within Canada Bay Locality. Heritage + Item - General : Domremy Convent Group (pub. 2013-07-19) 1:4.514 Fig 3. Locality of class 5 acidic sulphate soils. Fig 4. Heritage Conservation and Item-Domremy Convent. Surrounding vegetation.



8.0 DISCUSSION

8.1 The assessed trees are mostly outside of development and (117) one hundred and seventeen were assessed regarding the proposal. Of these trees the proposal indicates (6) six trees will be removed due to impacts by the new driveway access and the new building.

8.2 These (6)six trees have moderate value with tree 67 Callistemon viminalis (Red Bottlebrush) having a cavity and some structural issue, tree 72 Lophostemon confertus (Brush box) has a moderate to high value and 70-73 have moderate value and all have been heavily pruned. Tree 70 Jacaranda mimosifolia (Jacaranda) and tree 71 Brachychiton acerifolius (Illawarra flame tree). Tree 71 has been very damaged by heavy pruning with a 300mm cut across its stem at four (4) metres height from base. Trees 701,72&73 are mature age trees and have had the un-tolerable conditions (locality) of the school courtyard with compaction and typical school wear damage. Tree 73 has asphalt surrounding its rootzone and would continue to degrade without continuous maintenance.

8.3 A replenishment of these trees would be suited according to the tree management plan with six indigenous new plant stock of similar species selected according to <u>As2303 2015 Tree stock for</u> <u>Landscape Use</u>.

8.4 For the trees located adjacent these developed areas we propose tree protection and additional Tree Fence or Trunk Protection. This will include the trees within the northern side of the new carpark. These consist of two high value Phoenix canariensis (Phoenix palms) numbered 37&38 which will have some encroachment to their TPZ. Trees 31,32,33,34,35,36,41 have impacts to their TPZ which will include excavation and construction of the carpark. The table 2 indicates trees impacted and whether sensitive construction techniques, replenishment will be required.

8.5 Trees 44&45 will have impacts to their canopy and root system of less than ten percent but must be protected and pruned with an AQF Level 5 arborist present. This supervisory requirement will assist in the pruning of branches less than 40mm in diameter according to AS4373 2007 *Pruning of Amenity Trees.* As the road may access the TPZ area root pruning would be suitable with an AQF level 5 arborist certifying roots are cut cleanly prior to the installation of the road works. Tree trunk and canopy protection would be suitable, utilising hardwood lengths placed along their trunks vertically with 150mm air gaps and canopy protection of hessian adjacent there access. This can be reinforced with steel mesh panelling to restrict access into the TPZ. Inside the TPZ mulch of 150mm depth and clean certified mulch would be specified for ground protection.

8.6 TABLE 2. Trees with TPZ encroachment

Tree No.	Impacts	Tree Replenishment/Works Requirements
1	Excavation and construction of the carpark	Sensitive construction techniques where encroaching greater than 10%.
31,32,33,34,35,36,37,38,41	Excavation and construction of the carpark	Sensitive construction techniques where encroaching greater than 10%.
39,40	Remove impacted 100% by new access driveway to carpark.	Replenish (2) two trees with indigenous species or similar species.
44&45	Retain impacted greater than 10% by new access driveway to carpark.	Retain trees and utilise tree canopy and trunk protection.
67&68	Encroachment less than 10%	Minor pruning of canopy and ground and trunk protection installed.
70,71,72,73.	Remove impacted 100% by new building.	Replenish four trees indigenous species or similar species.
103	Construction of footings.	Sensitive construction techniques where encroaching greater than 10%.

9.0 HOLDING POINT

REQUIREMENTS PRIOR TO THE COMMENCEMENT OF ANY WORKS, INCLUDING DEMOLITION

- 1.1 The project arborist is to Mark the proposed trees to be removed with a waterproof marker at a visible height with a yellow cross.
- 1.2 Removal of Trees 39,40,70,71,72&73 by a Certified 3 arborist.
- 1.3 Any pruning greater than 40mm within TPZ of preserved trees will need to be cut cleanly under supervision of an AQF Level 5 Arborist. This will include clearances and crown canopy modification of any type.
- 1.4 Certification of tree protection as per Tree Protection Plan by AQF level 5 Arborist prior to any demolition, construction or re-landscaping.
- 1.5 No changes in soil level within TPZ of retained tree.
- 1.6 Root mapping for trees 1,31-38,4,44,45&103 prior to demolition and construction. Any roots greater than 40mm within TPZ but outside the SRZ of preserved trees will need to be cut cleanly under supervision of an AQF Level 5 Arborist.
- 1.7 Prohibitions are listed in appendix D 1,2,3&4 to be complied with and certified by an AQF level 5 arborist.
- 1.8 Replenishment of indigenous stock of 40litre potted volume selected from Appendix E list and planted according to the Tree Management Plan. (privy to production of a landscape plan)
- 1.9 Certifications of the compliance and bimonthly reports would be adequate for this development ensuring trees which are retained and preserved can be remediated if damage occurs. Remediation reports must be completed within one week of reporting in order to complete remedial works within the shortest timeframe and (likely) ensuring viability of trees.
- 1.10 The Project arborist name and contact details is to be made visible and legible with waterproof ink. with signage attached at 1.4m high to tree protection fencing, indicating the TPZ are not to be entered during or post construction unless supervised by the AQF level 5 arborist.

10.0 RECOMMENDATION

- 1. Removal of (6) six trees numbered; 39,40,70,71,72&73.
- 2. Completion of holding points 1.1, 1.2, 1.3, 1.4, 1.5, 1.6, 1.7, 1.8., 1.9. & 1.10
- 3. Root mapping of trees 1,31-38,41,44,45 &103 prior to construction.

To assist in the trees being managed competently the following recommendation is given: In maintaining the quality of the contractor selected to maintain the work in accordance

with AS/4743-2007 Pruning of Amenity Trees and Work safe "The Guide". The owner

should engage a contractor from the following associations; a registered current member

of Tree Contractors Association Australia (TCAA) or Arborists Australia (AA) must complete

the works.

11.0 GLOSSARY

Crown: The width of the foliage in the upper canopy of the assessed tree to the four cardinal points.

Crown lifting means the removal of the lower branches of the tree

Crown thinning means the portion of the tree consisting of branches and leaves and any part of the stem from which branches arise.

Drip line: Where the canopy releases water shed from the foliage during precipitation.

DBH/Diameter: Diameter of trunk at 1.4meters in height of assessed tree.

Dead wooding means the removal dead branches from a tree.

Dieback: Tree deterioration where the branches and leaves die.

Flush cut: A cut that damages or removes the branch collar or removes the branch and stem tissue and is inconsistent with the branch attachment as indicated by the bark branch ridge.

Genus/ Species: The Genus and species of each tree has been identified using its scientific name. Where the species name is not known the letters species is used. The common name for trees may vary considerably in each area of geographical differences and so will not be used in the field survey.

Height: Height has been estimated to + / - 2 meters.

ISA: International Society of Arboriculture.

Maturity: Tree maturity has been assessed as over mature (last one third of life expectancy), mature (one third to two thirds life expectancy) and semi mature (less than one third life expectancy).

Remedial (restorative) pruning: includes: Removing damaged, deadwood; trimming diseased or infested branches. Trimming branches back to undamaged tissue in order to induce the production of shoots from latent or adventitious buds, from which a new crown will be established.

SRZ- Structural Root Zone: An area within the trees root zone in which roots stabilize the tree. Roots cut in this zone can cause instability and lead to anchorage loss.

Structural Integrity: Describes the internal supporting timber. (Substantial to frail)

TULE- Tree Useful Life Expectancy: An estimation of the trees useful life expectancy using appropriate industry methods with an inspection regime.

TPZ- Tree Protective Zone: This zone should be considered as optimal for tree growth and sustainability however the size of the zone is subjective and should be reassessed when individual design and construction methods are being discussed.

Tree Age: Trees have either been assessed as mature, immature or semi-mature.

Tree Numbering: All trees listed in the tree survey have been numbered and plotted

Vigor: This is an indication of the tree health. Trees have either been assessed as Good Vigor, Normal Vigor or Low Vigor.

12.0 BIBLIOGRAPHY

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WEBSITE

http://maps.six.nsw.gov.au/ https://www.planningportal.nsw.gov.au

APPENDIX A TULE – TREE USEFUL LIFE EXPECTANCY

 Table 1 Revised 14.4.14 ADAPTED FROM JEREMY BARREL (SULE) FOR TCAA CLIMBING CONSULTANT ARBORISTS

	1 Long TULE	2 Medium TULE	3 Short TULE	4 Remove	5.No Potential for Retention REMOVE IMMEDIATELY	6 Small, Young or Regularly clipped
	Trees that appeared to be retainable at the time of assessment for more than 40 years with low level of risk	Trees that appeared to be retainable at the time of assessment for 15 to 40 years with and with low to medium level risk	Trees that appeared to be retainable at the time of assessment for 5 to 15 years with medium to high level of risk	Trees that should be removed within the next 5 years High to Very high level of risk	Trees that must be removed immediately. Very high to Extreme level of risk	Trees that can be easily transplanted or replaced.
Α	Structurally sound trees located in positions that can accommodate future growth	Trees that may only live for between 15 and 40 more years	Trees that may only live for between 5 and 15 more years	Dead, dying, suppressed or declining trees through disease or inhospitable conditions.	Dead, dying or declining trees diseased or inhospitable conditions.	Small trees less than 5 meters in height
В	Trees that could be made suitable for retention in the long term by Intervention Works.	Trees that may live for more than 40 years, but would need to be removed for safety or Nuisance reasons	Trees that may live for more than 15 years, but would need to be removed for safety or nuisance reasons	Dangerous trees through instability or recent loss of adjacent trees	Dangerous trees through instability or recent loss of adjacent trees	Young trees less than 15 years old but over 5 meters in height
с	Trees of special significance for historical, commemorative or rarity reasons that would warrant extraordinary efforts to secure their long term retention	Trees that may live for more than 40 years, but should be removed to prevent interference with more suitable individuals or to provide space for new planting	Trees that may live for more than 15 years, but should be removed to prevent interference with more suitable individuals or to provide space for new planting	Dangerous trees through structural defects including cavities, decay, included bark, wounds or poor form	Dangerous trees through structural defects including cavities, decay, included bark, wounds or poor form	Trees that have been regularly pruned to artificially control growth
D		Trees that could be made suitable for retention in the medium term by Intervention Works.	Trees that require substantial Intervention Works, and are only suitable for retention in the short term	Damaged trees that are clearly not safe to retain	Damaged trees that are clearly not safe to retain and must be removed immediately	
E				Trees that may live for more than 5 years, but should be removed to prevent interference with more suitable individuals or to provide space for new planting	High Toxicity Allegan trees, asthmatic and poisonous trees and must be removed immediately.	
F				Trees that may cause damage to existing structures within 5 years	OTHER with legitimate explanation to be removed immediately	
G				Trees that will become dangerous after removal of other trees for reasons given in 1A-1F		
INSPECTI ON FREQUE NCY	Inspection frequency 1-5 Years by competent inspector unless event monitored.	Inspection frequency 1-5 Years by competent inspector unless event monitored.	Inspection frequency 1-3 years by competent inspector unless event monitored.	Inspection frequency to 1 year by competent inspector unless event monitored.	1-7 days by competent inspector and event monitored	Inspection frequency Biannually by competent inspector

Arborist Impact Assessment and Tree Management Plan APPENDIX B HEALTH & STRUCTURAL CONDITION OF TREE- Visual McArdle Arboricultural Consultancy Pty Ltd

Health & Structural Condition of Tree
1. J- Juvenile; im- Immature; SM-Semi- Mature; M-Mature
2. Excellent Condition
3. Good Condition but Poor Development / Habit
4. Dieback is more than 20%. 4b Epicpormics
5. Sparse Foliage Crown 5b Unbalanced Canopy
6. Physical Damage
7. Cavity
8. Lean
9. Heavily Pruned
10. Inclusions
11. Damage to roots
12. Insect Damage 12b Borers
13. Termite Damage
14. Fungal Attack
15. Parasitic Vine Present
16. Damage by Climbing Plant
17. Habitat Tree
18. Endangered Species
19. Endangered community

Developed by Claus Mattheck in: *The Body Language of Trees*(1994), which have adapted versions from Hornsby Shire Council.

APPENDIX C RETENTION VALUES

TABLE 3 - DETERMINING LANDSCAPE SIGNIFICANCE RATING

RATING	HERITAGE VALUE	ECOLOGICAL VALUE	AMENITY VALUE	
	The subject tree is listed as a Heritage Item under the Local Environment Plan (LEP) with a local, state or national level of significance or is listed on Council's Significant Tree Register	The subject tree is scheduled as a Threatened Species as defined under the Threatened Species Conservation Act 1995 (NSW) or the Environmental Protection and Biodiversity Conservation Act 1999	The subject tree has a very large live crown size exceeding 300m ² with normal to dense foliage cover, is located in a visually prominent position in the landscape, exhibits very good form and habit typical of the species	
1. SIGNIFICANT	The subject tree forms part of the curtilage of a Heritage Item (building /structure /artefact as defined under the LEP) and has a known or documented association with that item	The tree is a locally indigenous species, representative of the original vegetation of the area and is known as an important food, shelter or nesting tree for endangered or threatened fauna species	The subject tree makes a significant contribution to the amenity and visual character of the area by creating a sense of place or creating a sense of identity	
	The subject tree is a Commemorative Planting having been planted by an important historical person (s) or to commemorate an important historical event	The subject tree is a Remnant Tree, being a tree in existence prior to development of the area	The tree is visually prominent in view from surrounding areas, being a landmark or visible from a considerable distance.	
2. VERY HIGH	The tree has a strong historical association with a heritage item (building/structure/artefact/garden etc) within or adjacent the property and/or exemplifies a particular era or style of landscape design associated with the original development of the site.	The tree is a locally-indigenous species, representative of the original vegetation of the area and is a dominant or associated canopy species of an Endangered Ecological Community (EEC) formerly occurring in the area occupied by the site.	The subject tree has a very large live crown size exceeding 200m ² ; a crown density exceeding 70% (normal-dense), is a very good representative of the species in terms of its form and branching habit or is a sethetically distinctive and makes a positive contribution to the visual character and the amenity of the area	
3. HIGH	The tree has a suspected historical association with a heritage item or landscape supported by anecdotai or visual evidence	The tree is a locally-indigenous species and representative of the original vegetation of the area and the tree is located within a defined Vegetation Link / Wildlife Corridor or has known wildlife habitat value	The subject tree has a large live crown size exceeding 100m ² ; The tree is a good representative of the species in terms of its form and branching habit with minor deviations from normal (e.g. crown distortion/suppression) with a crown density of at least 70% (normal); The subject tree is visible from the street and surrounding properties and makes a positive contribution to the visual character and the amenity of the area	
•	The tree has no known or suspected historical association, but	The publicit time is a non-local native or exotic species that is	The subject tops has a medium live crown size acceeding 40m ⁵ The tree is a fair representative of the spaces, emiliating moderne, deviations from typical form (distortion/suppression etc) with a crown density of more than 50% (fainning to normal); and	
MODERATE	does not detract or diminish the value of the item and is sympathetic to the original era of planting.	protected under the provisions of this DCP :-	The tree is visible from surrounding properties, but is not visually prominent, - visw may be partially obscured by other visibility built forms. The tree makes a fair contribution to the visual character and amenty of the area.	
. 5. LOW	The subject tree detracts from heritage values or diminishes the value of a heritage item	The subject tree is scheduled as exempt (not protected) under the provisions of this DCP due to its species, nuisance or position relative to buildings or other structures.	The subject tree has a small live crown size of less than 40m ² and can be replaced within the short term (5-10 years) with new tree planting	
5. Very Low	The subject tree is causing significant damage to a heritage Item.	The subject tree is lsted as an Environment Weed Species in the Leichhardt Local Government Area, being invasive, or is a known nuisance species.	The subject tree is not visible from surrounding properties (visibility obscured) and makes a negligible contribution or has a negative impact on the amenity and visual character of the area. The tree is a poor representative of the species, showing significant deviations from the typical form and branching habit with a crown density of less than 50% (sparse).	
7. INSIGNIFICANT	The tree is completely dead and has no visible habitat value	The tree is a declared Noxious Weed under the Noxious Weeds Act (NSW) 1993 within the relevant Local Government Area.	The tree is completely dead and represents a potential hazard.	

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DETERMINING THE RETENTION VALUE OF TREES ON DEVELOPMENT SITES EARTHSCAPE HORTICULTURAL SERVICES December 2011

RETENTION VALUE	RECOMMENDED ACTION		
"High"	 These trees considered worthy of preservation; as such careful consideration should be given to their retention as a priority. Proposed site design and placement of buildings and infrastructure should consider the Tree Protection Zones as discussed in the following section to minimise any adverse impact. In addition to Tree Protection Zones, the extent of the canopy (canopy dripline) should also be considered, particularly in relation to high rise developments. Significant pruning of the trees to accommodate the building envelope or temporary scaffolding is generally not acceptable. 		
"Moderate"	 The retention of these trees is desirable. These trees should be retained as part of any proposed development if possible, however they trees are considered less critical for retention. If these trees must be removed, replacement planting should be considered in accordance with Council's Tree Replacement Policy to compensate for loss of amenity. 		
 These trees are not considered to worthy of any special measures to en their preservation, due to current health, condition or suitability. They do have any special ecological, heritage or amenity value, or these values a substantially diminished due to their SULE. These trees should not be considered as a constraint to the future development of the site. 			
"Very Low"	 These trees are considered potentially hazardous or very poor specimens, or may be environmental or noxious weeds. The removal of these trees is therefore recommended regardless of the implications of any proposed development. 		

APPENDIX D TREE PROTECTION

Extract from Australian Standard AS4970 2009 Protection of trees on development sites 4.5 OTHER TREE PROTECTION MEASURES

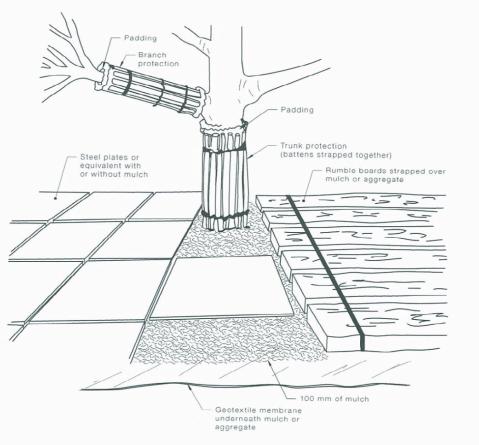
When tree protection fencing cannot be installed due to restricted access e.g. tree located along side an access way or requires temporary removal, other tree protection measure should be used, including those set out below;

4.5.2 TRUNK AND BRANCH PROTECTION see fig4.

4.5.3 GROUND PROTECTION

If temporary access for machinery is required within the TPZ, ground protection measure will be required to prevent compaction in the root zone. Measures may include permeable membrane such as geotextile fabric beneath a layer of mulch (100mm) or crushed rock below rumble boards as per fig 4.

Examples of Trunk, Branch and ground protection



NOTES:

- 1 For trunk and branch protection use boards and padding that will prevent damage to bark. Boards are to be strapped to trees, not nailed or screwed.
- 2 Rumble boards should be of a suitable thickness to prevent soil compaction and root damage.

FIGURE 4 EXAMPLES OF TRUNK, BRANCH AND GROUND PROTECTION

4.4.5 Installing underground services within TPZ

"All services should be routed outside the TPZ. If underground services must be routed within the TPZ, they should be installed by directional drilling or in manually excavated trenches. The directional drilling bore should be at least 600 mm deep. The project arborist should assess the likely impacts of boring and bore pits on retained trees. For manual excavation trenches the project arborist should advise on roots to be retained and should monitor the works. Manual excavation may include the use of pneumatic and hydraulic tools.

McArdle Arboricultural Consultancy Pty Ltd

PROHIBITIONS

1. The following activities shall not be carried out within any Tree Protection Zone:

- I. Disposal of chemicals and liquids (including concrete and mortar slurry, solvents, paint, fuel or oil);
- ii. Stockpiling, storage or mixing of materials;
- iii. Refuelling, parking, storing, washing and repairing tools, equipment, machinery and vehicles;
- iii. Disposal of building materials and waste;

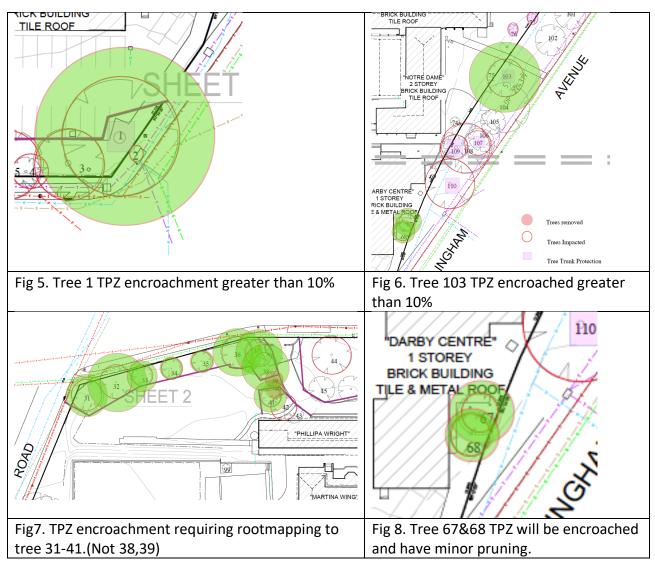
2. The following activities shall not be carried out within any Tree Protection Zone unless under the supervision of the Project Arborist:

- A. Increasing or decreasing soil levels (including cut and fill);
- B. Soil cultivation, excavation or trenching;
- C. Placing offices or sheds;
- D. Erection of scaffolding or hoardings; and/or
- E. Any other act that may adversely affect the vitality or structural condition of the tree.

3.All work undertaken within or above a Tree Protection Zone shall be supervised by the Project Arborist. (See below fig5-8).

4. Excavation within the Tree Protection Zone of any tree to be retained shall:

A. Be undertaken using <u>non-destructive methods</u> (eg. an Airspade or by hand) to ensure no roots greater than 40mm in diameter are damaged, pruned or removed. All care shall be taken to preserve and avoid damaging roots; B.not occur within the Structural Root Zone.



Arborist Impact Assessment and Tree Management Plan APPENDIX E TREE PLANTING SPECIFICATIONS AND MAINTENANCE McArdle Arboricultural Consultancy Pty Ltd

Before planting, careful consideration should be given to the location of trees and shrubs to minimise future problems. Review <u>As2030 2015</u> for selection criteria of Planting Stock for Landscape Use. A basic guide for planting follows:

- Don't plant too close to buildings or in-ground pools or plant large trees too close together: Determine the height and canopy of trees when fully grown. Allow room for root growth (at least twice the height of the tree). Large trees should be planted at least three meters from buildings.
- 2. Check when planting under wires or over drainage lines: Determine the mature size of the tree and the size and nature of its root system.
- 3. Consider your neighbors when choosing plants: Consider the effect on neighbouring properties (i.e. shading, loss of views, impact on foundations, fences and services).
- 4. Use trees to provide your home with summer shade and/or winter sun: Plant deciduous trees (suitable to the climate and soils of this Shire). Consider the summer and winter shadows of evergreen trees.
- 5. Don't grow climbers on trees: Climbers can strangle trees, leading to the tree's eventual death.
- 6. Retain and protect as many trees as possible when building or extending your home. (This will be a Council requirement).
- 7. Use locally native and non-invasive species in your garden: Increase the success rate of your garden. Attract native fauna to your garden. Reduce the amount of watering required.
- 8. Don't excavate or alter the ground level around trees: Can cause root damage or starving of the roots. Can cause limb drop, instability or tree death. Substantially altering soil level within three meters of the trunk is in breach of the Tree Preservation Order.
- 9. When buying plants, check their characteristics: Check on mature size, shade characteristics, potential for roots to cause damage, flowers, fruits and pollen, to determine their suitability.

Mature trees do need maintenance: Remove or trim misshapen branches. Check for fungal rots or other diseases. If in doubt, contact Council for a tree inspection or contact an experienced Arborist. Indiscriminate lopping can be dangerous to your safety and the health of the tree.

Varles Varles Street tree planting with hardwood stakes with pointed end clear of rootball Hesslan webbing thes Much placed clear of plant stem tapering

Staking of trees should be carried out similar to the diagram.

McArdle Arboricultural Consultancy Pty Ltd

Arborist Impact Assessment and Tree Management Plan APPENDIX F INDIGENOUS TREE REPLENISHMENT McArdle Arboricultural Consultancy Pty Ltd

Replacement Tree Species	Recommended Replacement Species	
Low Allergy Trees		
	<u>*Szygium smithii</u> Lilly Pilly	
<u>Agonis flexuosa</u> Willow Myrtle	<u>Tristaniopsislaurina</u> Water Gum	
<u>Araucaria heterophylla</u> Norfolk Is. Pine	<u>Corymbia exemia</u> Yellow Bloodwood	
<u>Bauhinia blakeana</u> Butterfly Tree	*Backhousia citriodora Lemon Scented	
<u>Eucalyptus spp.</u> Eucalyptus Trees	Myrtle	
<u>Grevillea robusta</u> Silky Oak	<u>*Elaeocarpusreticulatus</u> Blueberry Ash	
Hakea laurina Pincushion Plant	<u>*Waterhousia floribunda</u> Weeping Lilly	
<u>H. salicifolia</u> Willow Leaved Hakea	Pilly	
<u>Magnolia grandiflora</u> Bull Bay	<u>Syzygium leuhmannii</u> Riberry	
<u>Malus floribunda</u> Crab Apple	<u>Hymenosporumflavum</u> Native Frangipani	
<u>Melaleuca quinquenervia</u> Broad Leaved	<u>E. paniculata</u> Grey Ironbark	
Paperbark	<u>Eucalyptus microcorys</u> Tallowood	
<u>Nyssa sylvatica</u> Tupelo	<u>Eucalyptus leucoxylon</u> Yellow Gum	
<u>Pistaciachinensis</u> Pistachio	Eucalyptus crebra Narrow Leaved Ironbark	
<u>Prunus x blireana</u> Flowering Plum	<u>Syncarpia glomulifera</u> Turpentine	
<u>Szygium smithii</u> Lilly Pilly	<u>Lophostemon confertus</u> Brush Box	

• Recommended for this site.

Suitable Understory Plants		
Understory trees:	Understory shrubs	
<u>Pittosporum undulatum</u> Sweet	<u>Breynia oblongifolia</u> Coffee Bush	
Pittosporum	Pittosporum revolutum Rough-fruited	
<u>Elaeocarpus reticulatus</u> Blueberry Ash	Pittosporum	
<u>Allocasuarina torulosa</u> Forest Oak	Polyscius sambucifolia Elderberry Panax	
	Myrsine variabilis Muttonwood	

DISCLAIMER

McArdle Arboricultural Consulting Pty Ltd does not assume responsibility for liability associated with the tree on or adjacent to this project site, their future demise and/or any damage, which may result therefrom.

Any legal description provided to McArdle Arboricultural Consultancy Pty Ltd is assumed to be correct. Any titles and ownerships to any property are assumed to be good and sound. McArdle Arboricultural Consultancy Pty Ltd takes care to obtain all information from reliable sources. All data has been verified insofar as possible; however, the consultant can neither guarantee nor be responsible for the accuracy of information provided by others.

McArdle Arboricultural Consultancy's reports and recommendations shall not be viewed by others or for any other reason outside its intended target, either partially or whole, without the prior written consent of the consultant. Unauthorised alteration or separate use of any section of the report invalidates the whole report. McArdle Arboricultural Consultancy Pty Ltd cannot be held responsible for any consequences as a result of work carried out outside specifications, not in compliance with Australian Standards or by inappropriately qualified staff.

Sketches, diagrams, graphs, and photographs in this report, being intended as visual aids, are not necessarily to scale. All recommendations contained within this report represent the current industry best practice methods of inspection. McArdle Arboricultural Consultancy Pty Ltd shall not be required to give testimony or to attend court by reason of this report unless subsequent contractual arrangements are made, including payment of an additional fee for such services.

LIMITS OF OBSERVATION

McArdle Arboricultural Consultancy Pty Ltd makes every effort to accurately identify current tree health and safety issues. Results may or may not correlate to actual tree structural integrity. There are many factors that may contribute to limb or total tree failure. Not all these symptoms are visible. There can be hidden defects that may result in a failure even though it would seem that other, more obvious defects would be the likely cause of failure.

All standing trees have an element of unpredictable risk. McArdle Arboricultural Consultancy Pty Ltd endeavors to identify the risk that the tree represents; however a level of risk associated with every tree will remain. McArdle Arboricultural Consultancy Pty Ltd does not provide any warranty or guarantee that problems, deficiencies or failures with regard to the plant/s, property or building/s will not arise in the future.

Ongoing monitoring may foresee deterioration of a tree and allow remedial action to be taken to prevent injury or damage. The timing for re-inspection on individual trees is subjective and will vary however an annual inspection is advisable for trees in subsequent years.

FURTHER RESEARCH The report does not cover threatened, heritage or existing trees in relation to remnant forest. Further reporting may be considered as part of the relevantRISK ASSESSMENT.

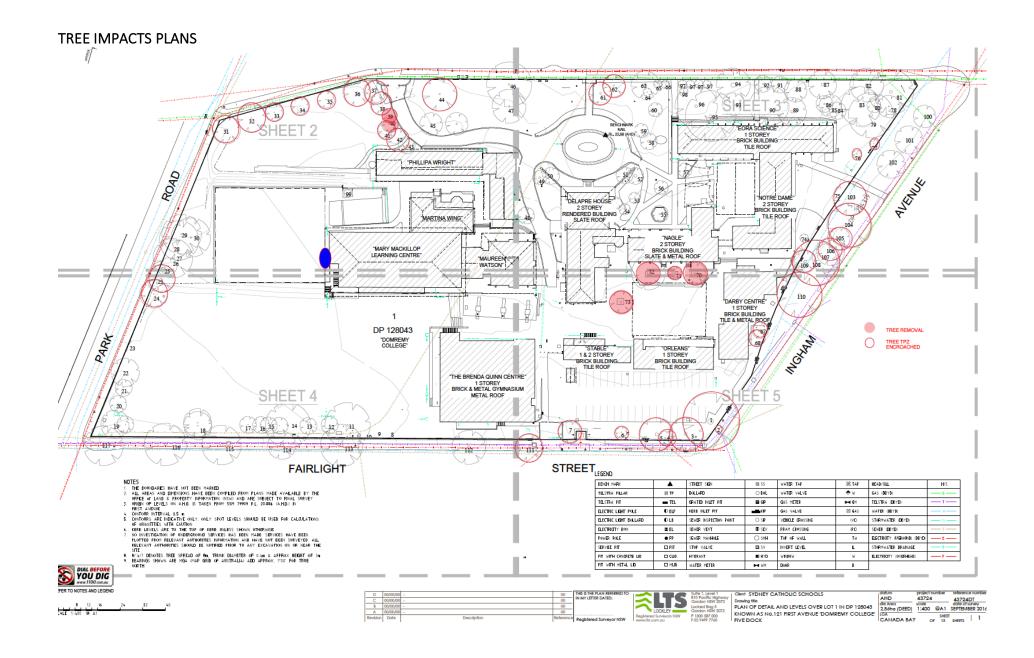
LIMIT OF OBSERVATIONS

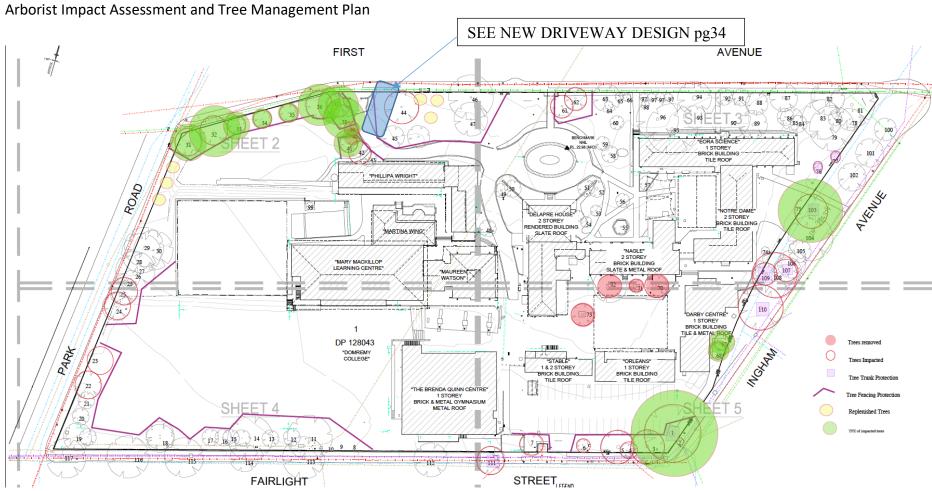
"There are many factors that may contribute to limb or total tree failure. Factors include, decay (in the trunk, crown or branch junctions), external damage to branches leading to decay, poor branch taper, included bark, root rot/ decay. Not all these symptoms are visible i.e. internal decay; of these some external symptoms may indicate the presence of deadwood but not the extent of decay. The most solid looking piece of timber may be riddled with breaks in continuity of growth caused by insect damage or poor pruning practices or other physical damage caused many years previous. Trees don't heal; they simply box in the damaged area ((CODIT) Compartmentalization of Decay In Trees.) and continue to expand in girth, completely disguising the fact that the branch or trunk has a hollow or decayed section. Having said this, not all areas, of decay past or present suggest a point of failure."

In addition to this information, other variables that can contribute to limb or total tree failure are tree species, wood densities, weight, age, location, exposure to the elements, soil types, disease and pests, birds using trees as habitat and food sources, termites causing structural problems and human influences such as, altered drainage, compaction or leaching of miner.

Tree Location Plan

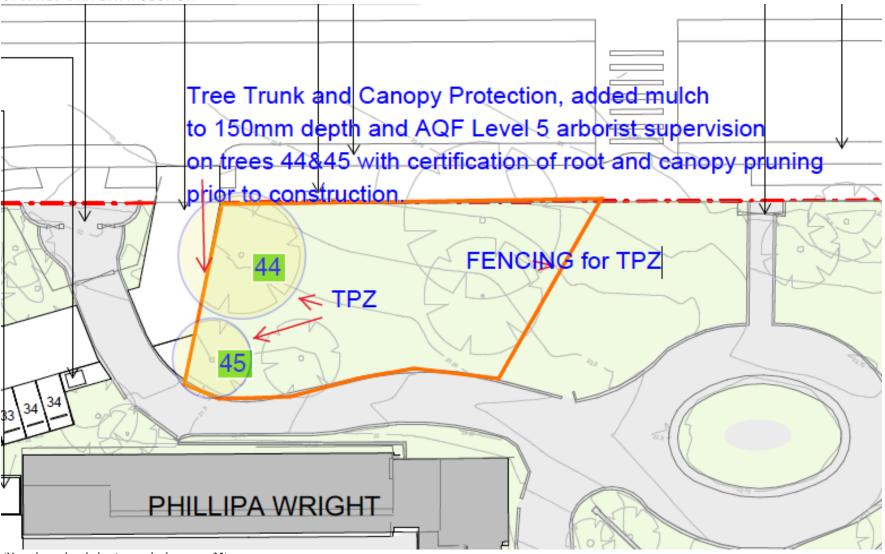






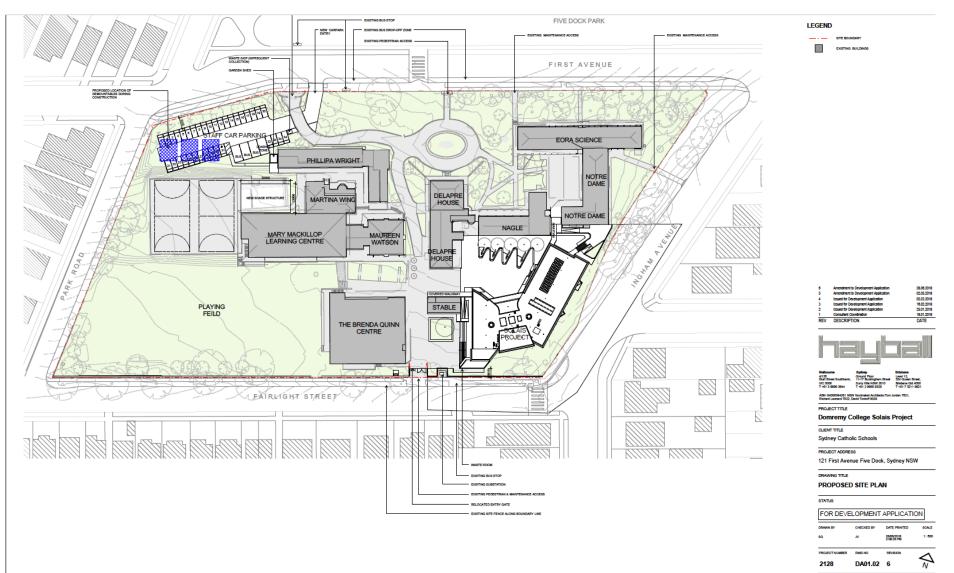
TREE MANAGEMENT PLAN

UPDATED DRIVEWAY SECTION



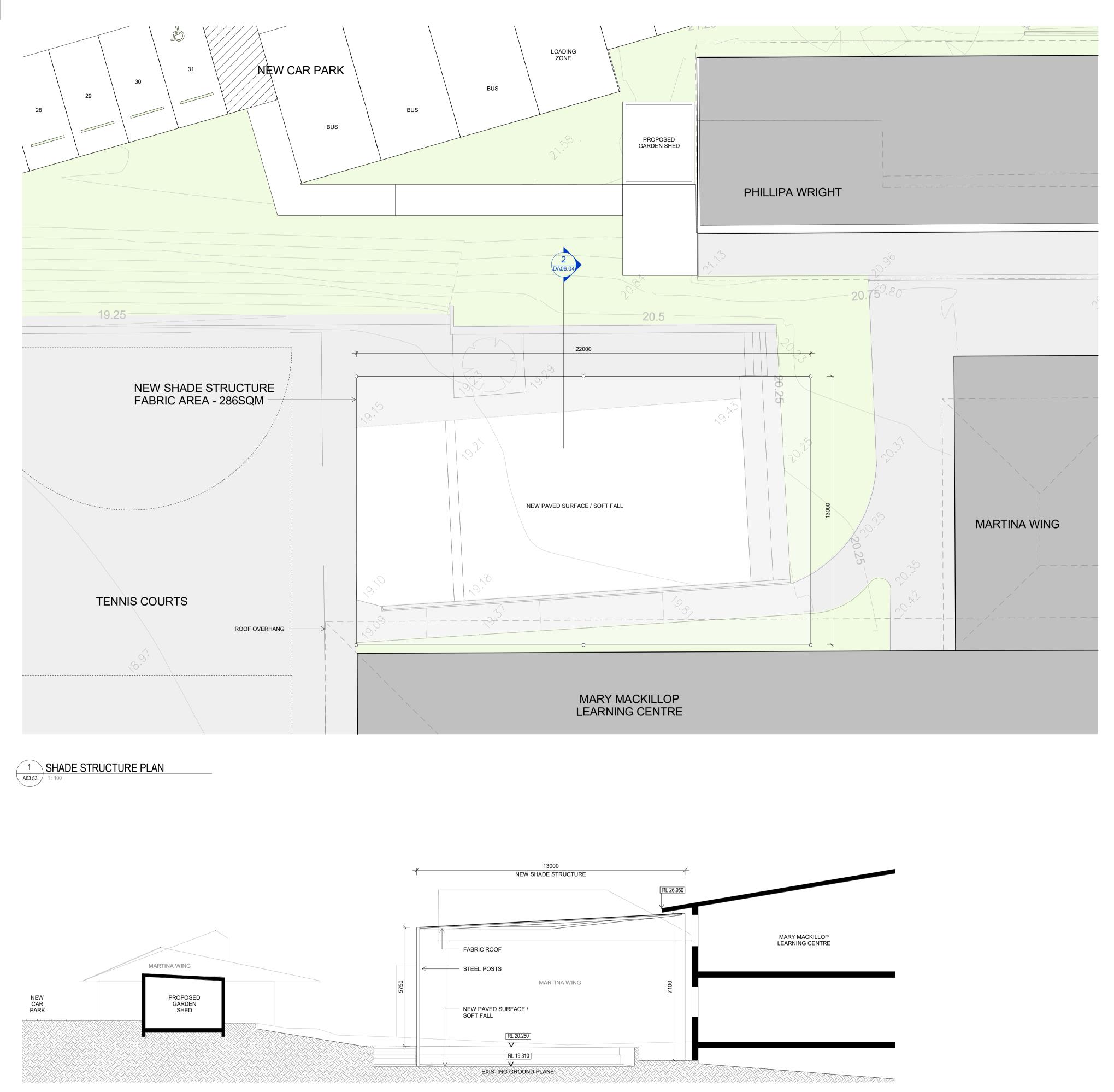
(Note the updated plan is attached on page 35).

UPDATED PLAN



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2 SHADE STRUCTURE SECTION DA06.04 1:100

Builders/Contractors shall verify job dimensions before any job commences. Figured dimensions shall take precedence over scaled work. Work shall also conform to the specification, other drawings and job dimensions. All shop drawings shall be submitted to the Architect/Consultant and manufacture shall not commence prior to the return of inspected shop drawings signed by the Architect/Consultant. © Copyright 2008 All rights reserved

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FOR DEVELOPMENT APPLICATION							

STATUS

SHADE STRUCTURE SECTION

DRAWING TITLE

121 First Avenue Five Dock, Sydney NSW

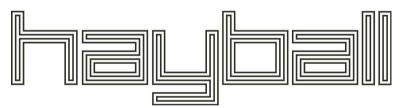
PROJECT ADDRESS

CLIENT TITLE Sydney Catholic Schools

Domremy College Solais Project

ABN: 84006394261 NSW Nominated Architects:Tom Jordan 7521, Richard Leonard 7522, David Tordoff 8028 PROJECT TITLE

MelbourneSydneyBrisbane4/135Ground FloorLevel 12,Sturt Street Southbank,11-17 Buckingham Street324 Queen Street,VIC 3006Surry Hills NSW 2010Brisbane Qld 4000T +61 3 9699 3644T +61 2 9660 9329T +61 7 3211 9821



Amendment to Development Application 28.06.2018 1 REV DESCRIPTION DATE



PDC Consultants Level 5, 104 Commonwealth Street Surry Hills NSW 2010 T: +61 2 7900 6514 ABN: 70 615 064 670

Ref: 0057r01v01

3/07/2018

Impact Group Level 1, 51 Walker Street North Sydney NSW 2060

Attention: Josh Partridge

RE: DOMREMY CATHOLIC COLLEGE - 121 FIRST AVENUE, FIVEDOCK (DA 2018/0076) LETTER OF RESPONSE TO COUNCIL

Dear Josh,

We refer to recent correspondence concerning the abovementioned development and in particular, the subject Development Application DA 2018 / 0076 which is currently under assessment by Canada Bay Council.

Council's Statutory Planner issued an email on the 17/05/2018 requesting clarification / additional information to be provided regarding a number of aspects of the proposed development, including aspects relating to the design of the proposed driveway onto First Avenue. In this regard, we confirm that we have taken Council's comments into consideration and now provide a response to each of Council's comments separately below. Our response is provided separately underneath each of Council's comments and is shown indented and in *italics*.

Council's Comment No. 1

Longitudinal sections are to be provided along the extreme wheel path of proposed driveway in First Avenue. The section shall extend from the centre line of the roadway and shall include all gradients including footpath cross fall to be at a maximum of 2.5%, change of grade and grade transition details and levels. It shall also include a standard layback crossing with a maximum of 100mm level difference from the invert of the gutter to top of layback. Layback levels shall be consistent with the detail survey levels.

A longitudinal section has been prepared in accordance with the above requirements, for the two (2) extreme wheel paths of the proposed access driveway onto First Avenue. These have been prepared by Enstruct Group and included in **Attachment 1** for reference.



Council's Comment No. 2

The driveway profile shall also demonstrate compliance with the scraping provisions of AS/NZS 2890.1:2004 based on the 85th percentile vehicles ground clearance templates.

As stipulated in AS/NZS 2890.1:2004 (AS 2890.1), the 85th percentile vehicle (B85) ground clearance template is to be used for domestic driveways only. Accordingly, for the purposes of a more conservative assessment and to ensure compliance with AS 2890.1, a ground clearance assessment was undertaken using the 99th percentile vehicle (B99) ground clearance template defined in AS 2890.1.

Our assessment was undertaken along each edge of the First Avenue access driveway using the two longitudinal sections provided in **Attachment 1**. The results of the vertical clearance test are included in **Attachment 2** and confirm the proposed access driveway complies with the relevant provisions of AS 2890.1, and that no scraping of the vehicle undercarriage will occur.

Council's Comment No. 3

Driveway entrance shall be perpendicular to the kerb and gutter alignment and should not be designed with kerb returns.

The Enstruct Group drawings included in **Attachment 1** confirm that the proposed access driveway onto First Avenue shall be constructed perpendicular to the kerb and gutter alignment, and will not incorporate kerb returns.

Council's Comment No.4

All redundant driveways shall be removed, and footway and footpath reinstated. Any redundant stormwater outlets shall also be removed.

All redundant driveways shall be removed, and footway and footpath reinstated. Any redundant stormwater outlets shall also be removed.

Separate to the above, we note that comments have been received from Council's tree officer and heritage advisor advising that the proposed driveway onto First Avenue should be relocated to ensure that Tree 38 is able to be retained. In response, we note that the alignment of the First Avenue driveway and internal roadway have been reconfigured to ensure that these are clear of Tree 38 and importantly, that Tree 38 is able to be retained. The revised arrangements are shown by the amended Site Plan, prepared by Hayball, included in **Attachment 3**.

The revised arrangements have also been assessed using swept path analysis for a 7.6 metre Toyota Coaster and 8.8 metre Medium Rigid Vehicle (MRV). The results are included in **Attachment 2** and confirm that satisfactory entry and exit movements will be achieved, clear of Tree 38. We do however note that access by an 8.8 metre MRV will only be permitted outside of school hours when the car park is vacant. This will ensure that there is ample space for an 8.8 metre MRV to turn around on-site as demonstrated by the swept path results.

An updated swept path of an 8.8 metre MRV accessing the waste collection area is also included in **Attachment 2** for reference. This confirms that satisfactory entry and exit movements will be achieved to the waste collection area, which would also occur outside of school hours.



We trust the above satisfactorily resolves all of the parking design concerns raised by Council. Please contact the undersigned should you have any queries or require anything further.

Yours sincerely,

Julius Boncato Traffic Engineer, PDC Consultants

Email: jboncato@pdcconsultants.com.au

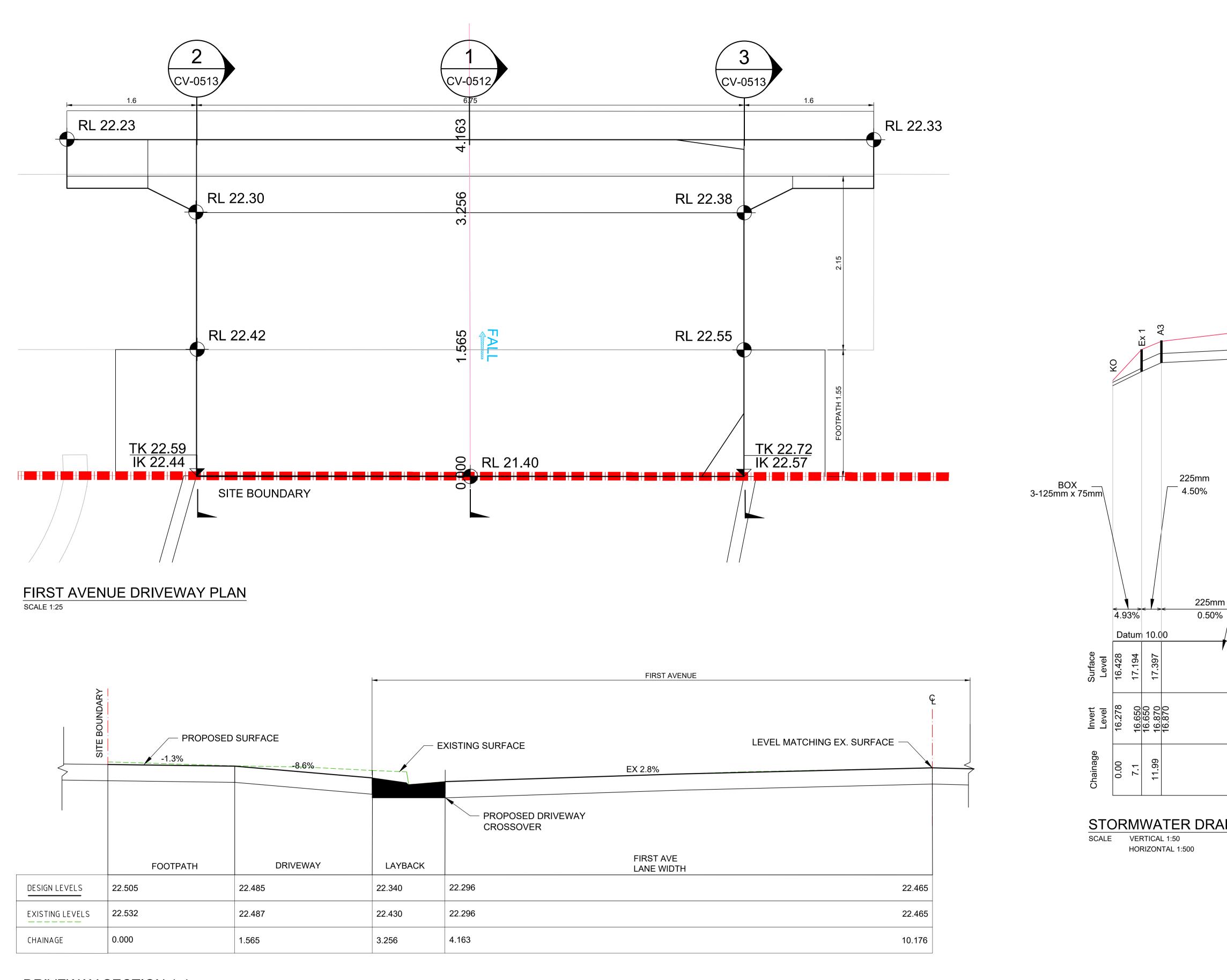
Attachments:

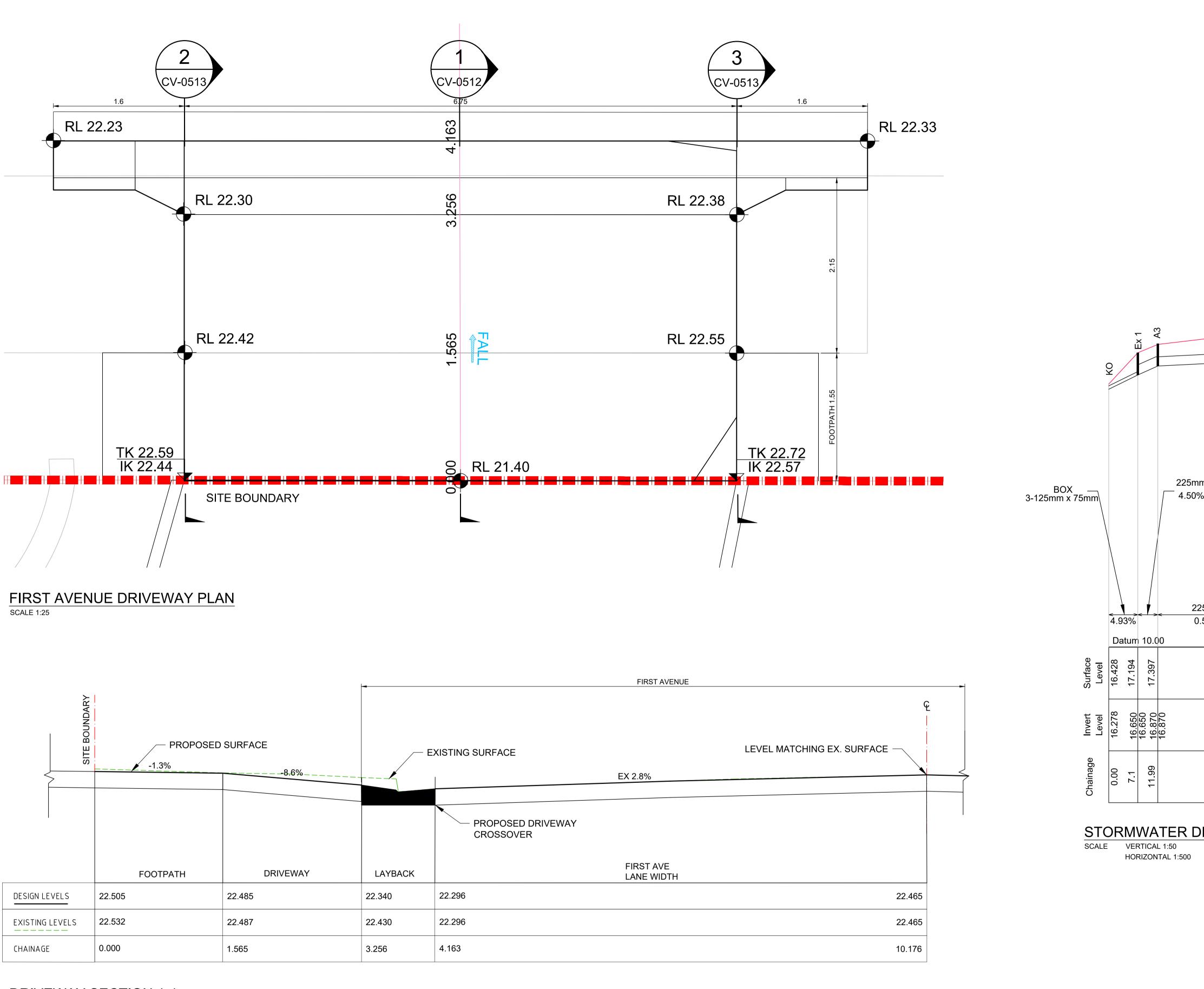
- 1) Civil Drawings of the Proposed Driveway onto First Avenue
- 2) Vertical Clearance Test & Swept Path Analysis Results

3) Amended Site Plan



Attachment 1





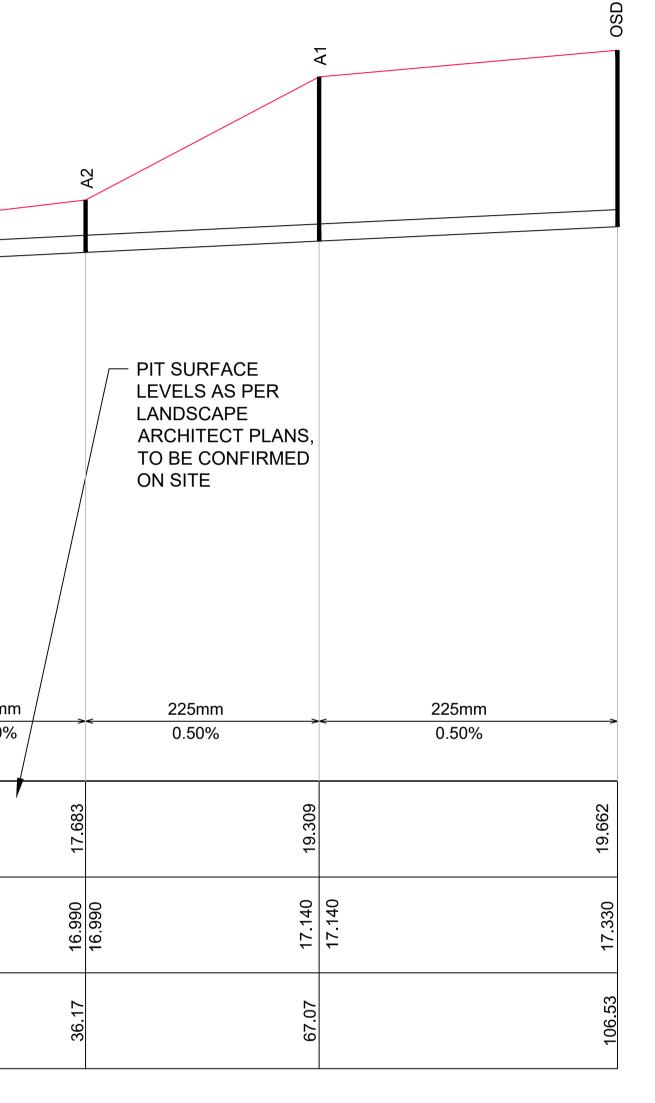
DRIVEWAY SECTION 1-1 SCALE 1:25

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enstruct group pty ltd	DOMREMY COLLEGE	drawing title SITEWORKS DETAILS	FOR	INFOF	RMATION	ONLY	
Level 4, 2 Glen Street Milsons Point NSW 2061 Australia	SOLAIS LAB PROJECT FIVE DOCK	SHEET 2	scale at A1 NTS	drawn by ML	checked MM	^{date} JUN-18	
Telephone (02) 8904 1444 Facsimile (02) 8904 1555 www.enstruct.com.au Construct			project no.		drawing no. CV-0512	rev.	2

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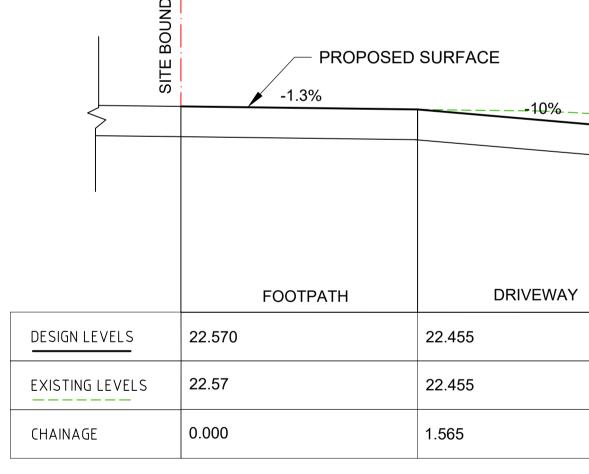
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DRIVEWAY SECTION 2-2 SCALE 1:25



NDARY			-		FIRST AVENUE	ę
SITE BOUNDARY	PROPOSI	ED SURFACE	E	EXISTING SURFACE	EX 2.5%	LEVEL MATCHING EX. SURFACE
				PROPOSED DRIVEWAY CROSSOVER		
	FOOTPATH	DRIVEWAY	LAYBACK		FIRST AVE LANE WIDTH	
DESIGN LEVELS	22.440	22.420	22.300	22.225		22.404
EXISTING LEVELS	22.440	22.487	22.430	22.225		22.404
CHAINAGE	0.000	1.565	3.256	4.163		10.176

	-		FIRST AVENUE		
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		PROPOSED DRIVEWAY CROSSOVER			
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	22.430	22.330		22.523	
	3.256	4.163		10.176	

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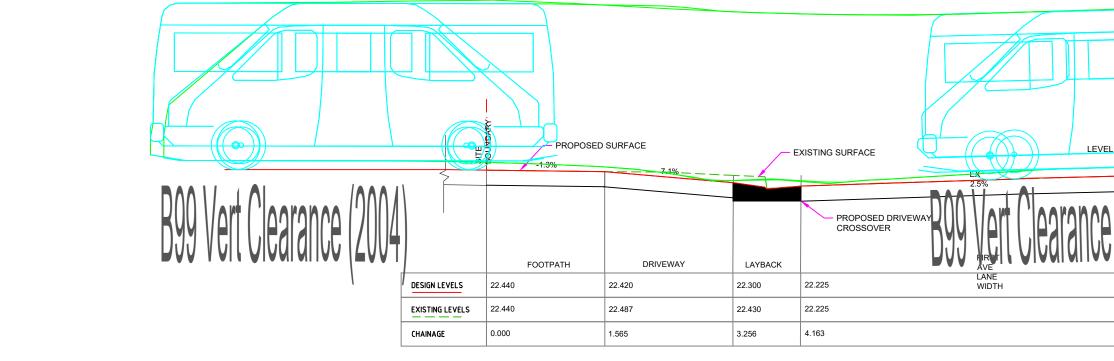
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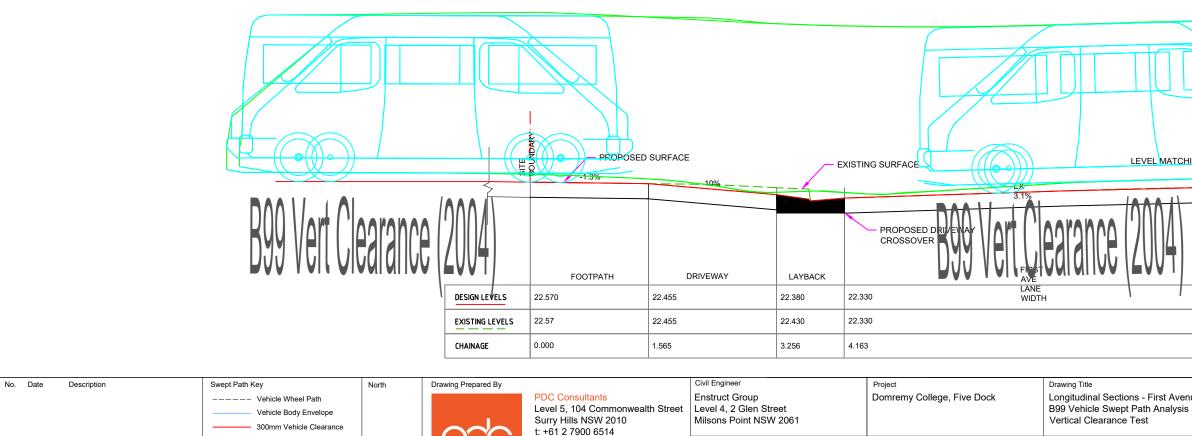


Attachment 2

DRIVEWAY SECTION 2-2







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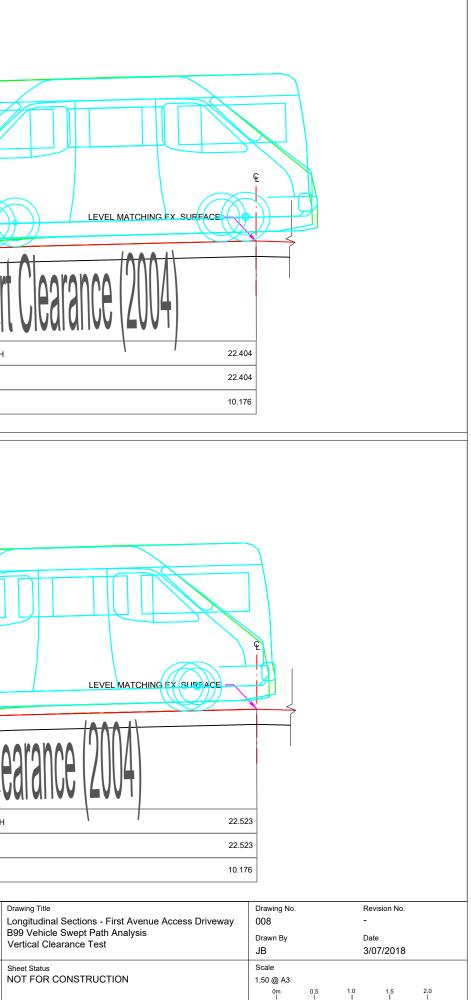
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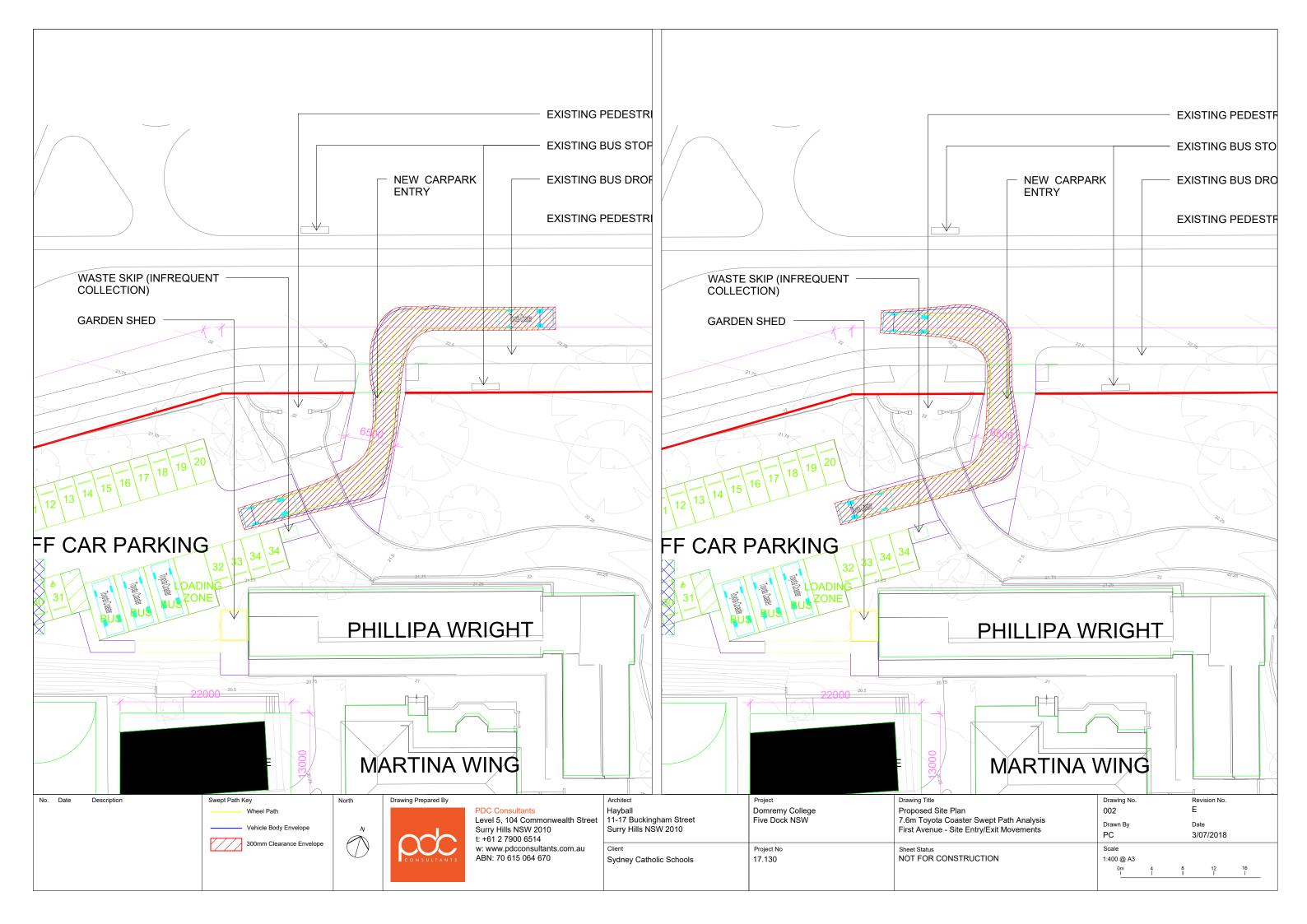
Client

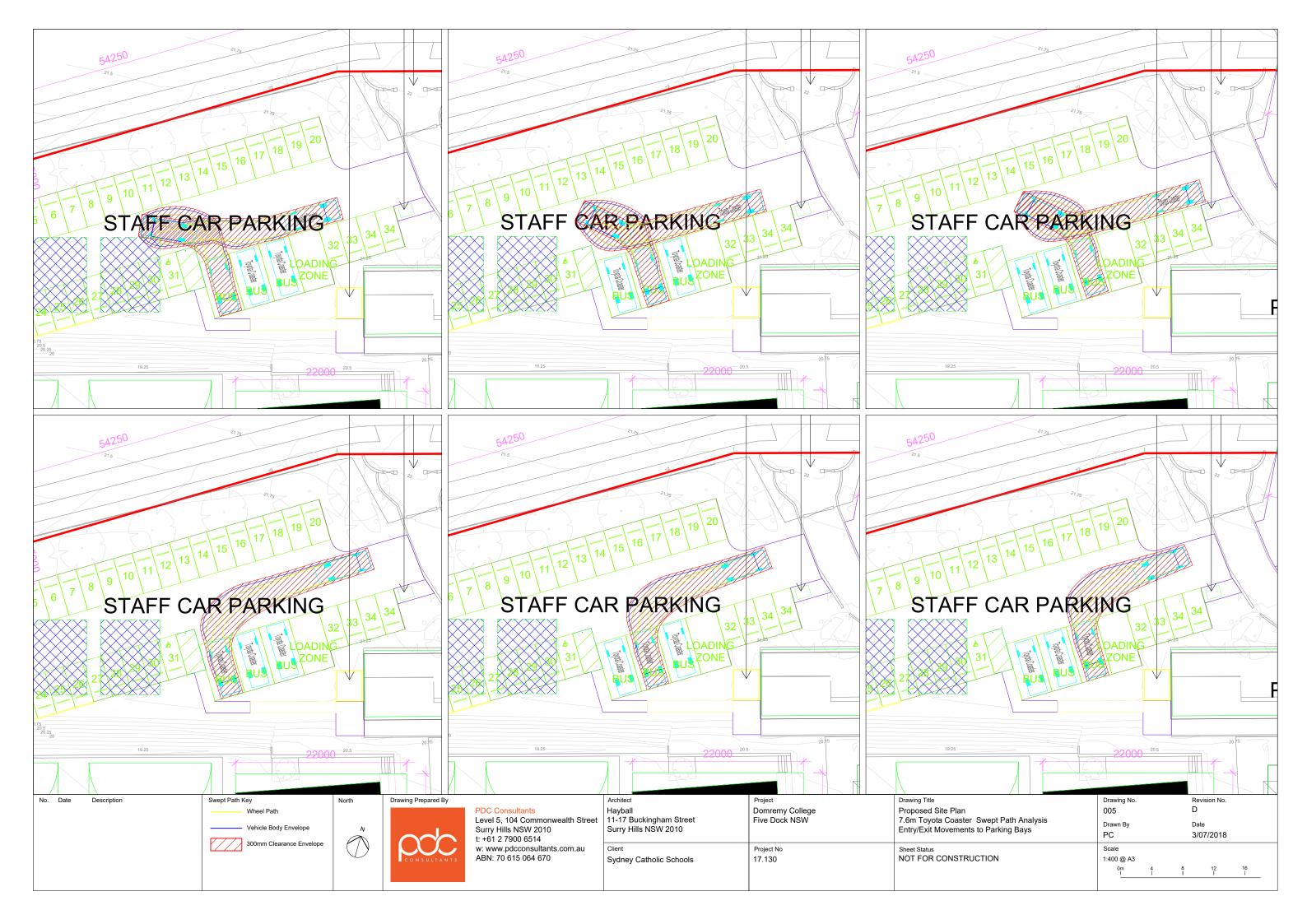
Sydney Catholic Schools

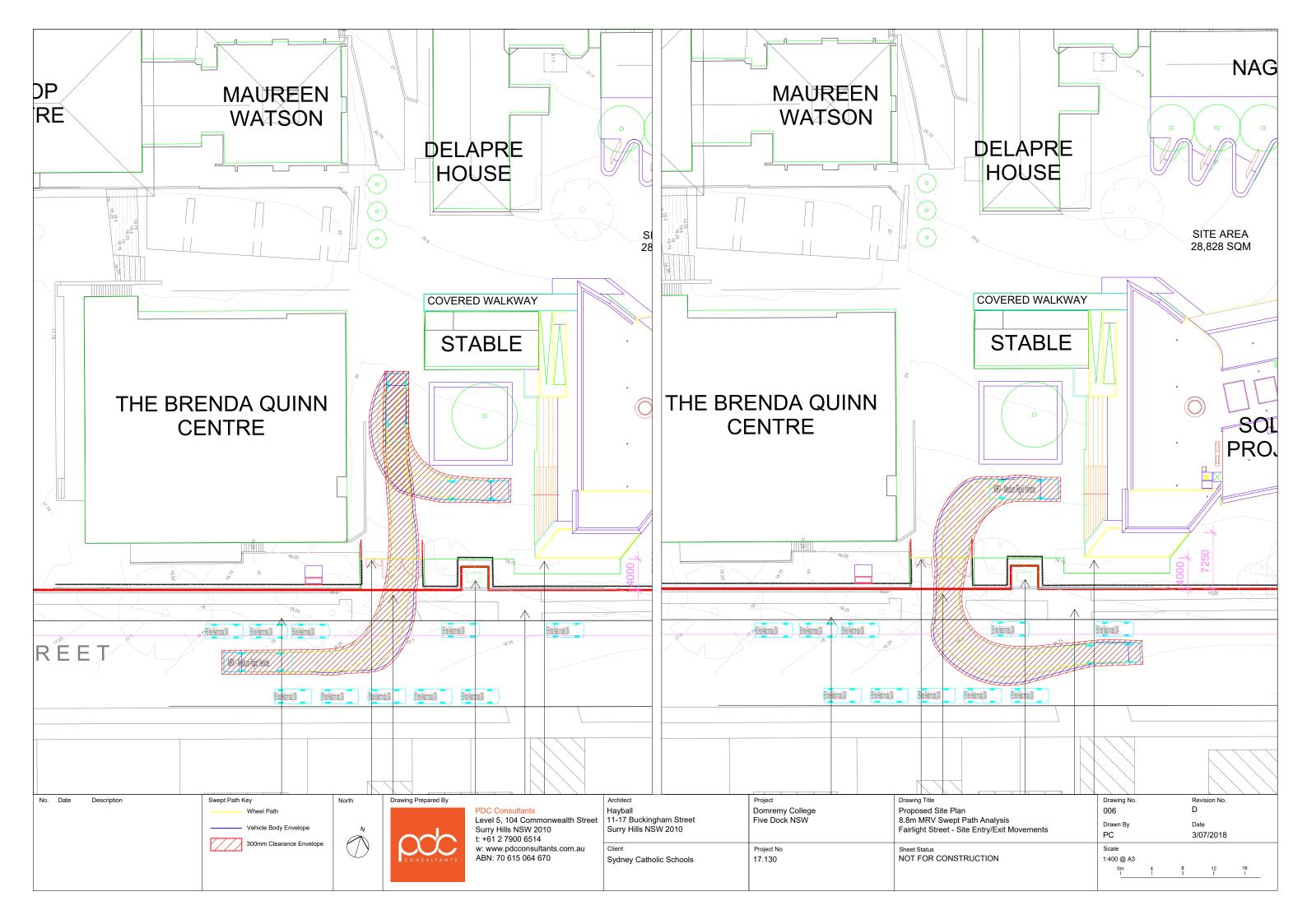
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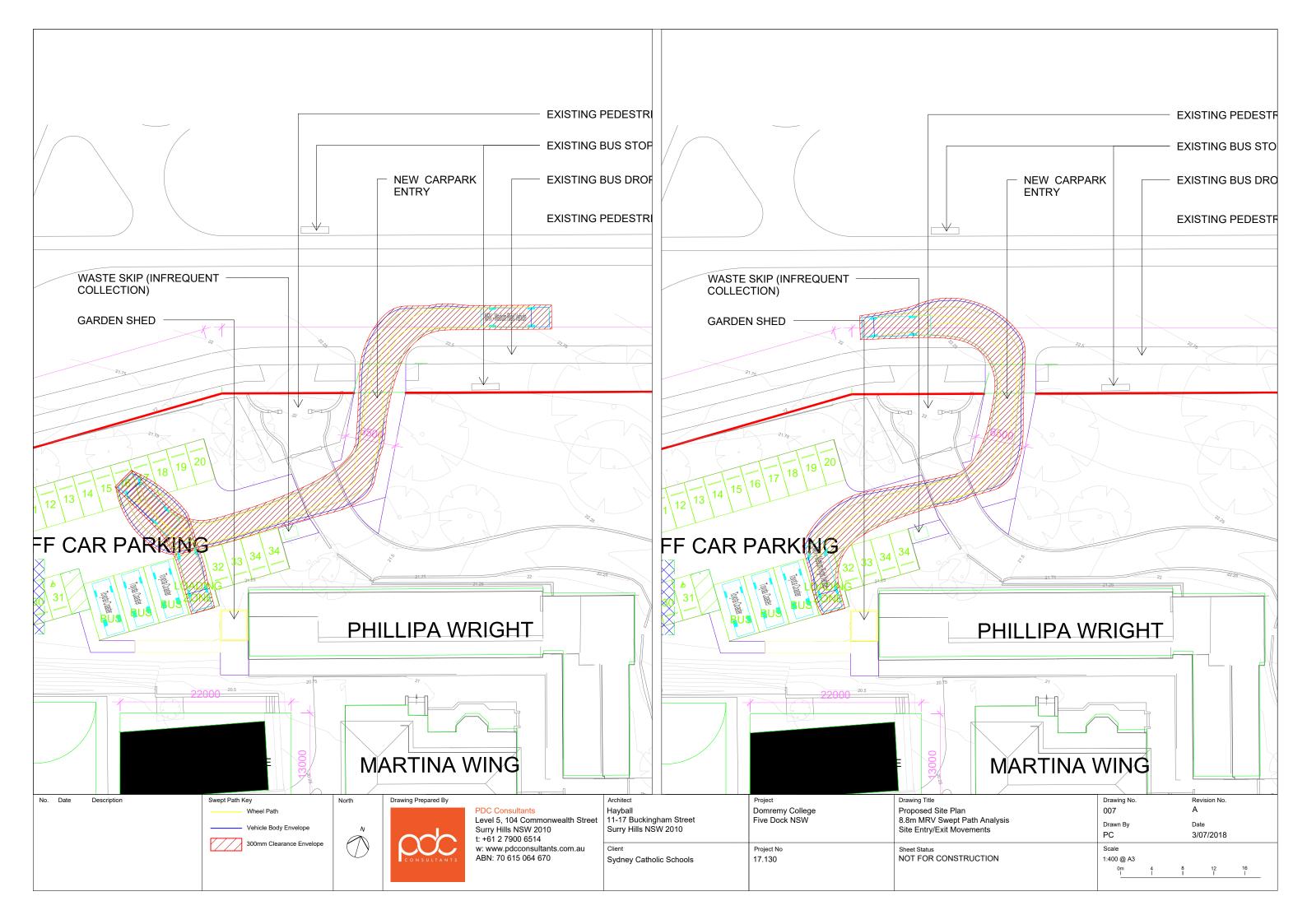
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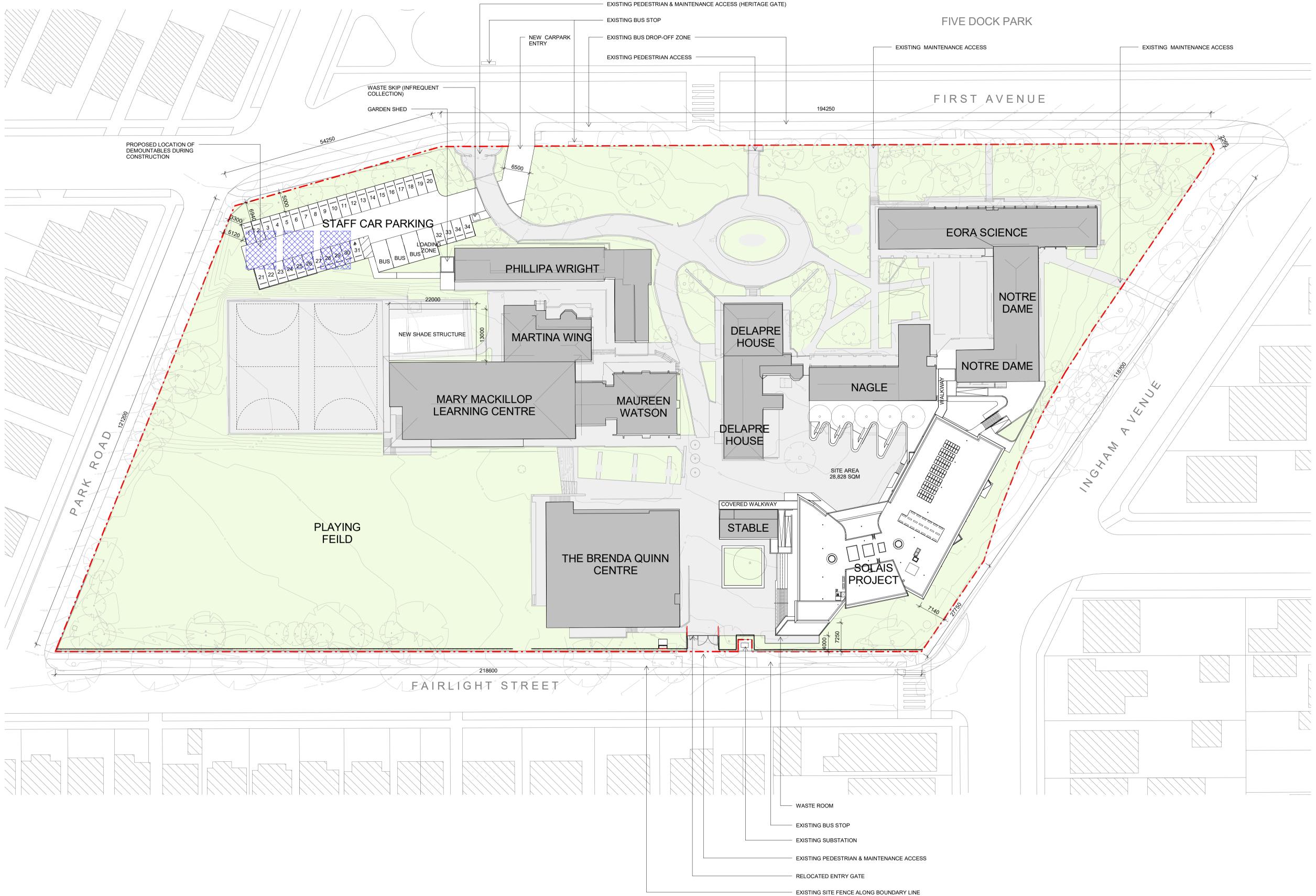


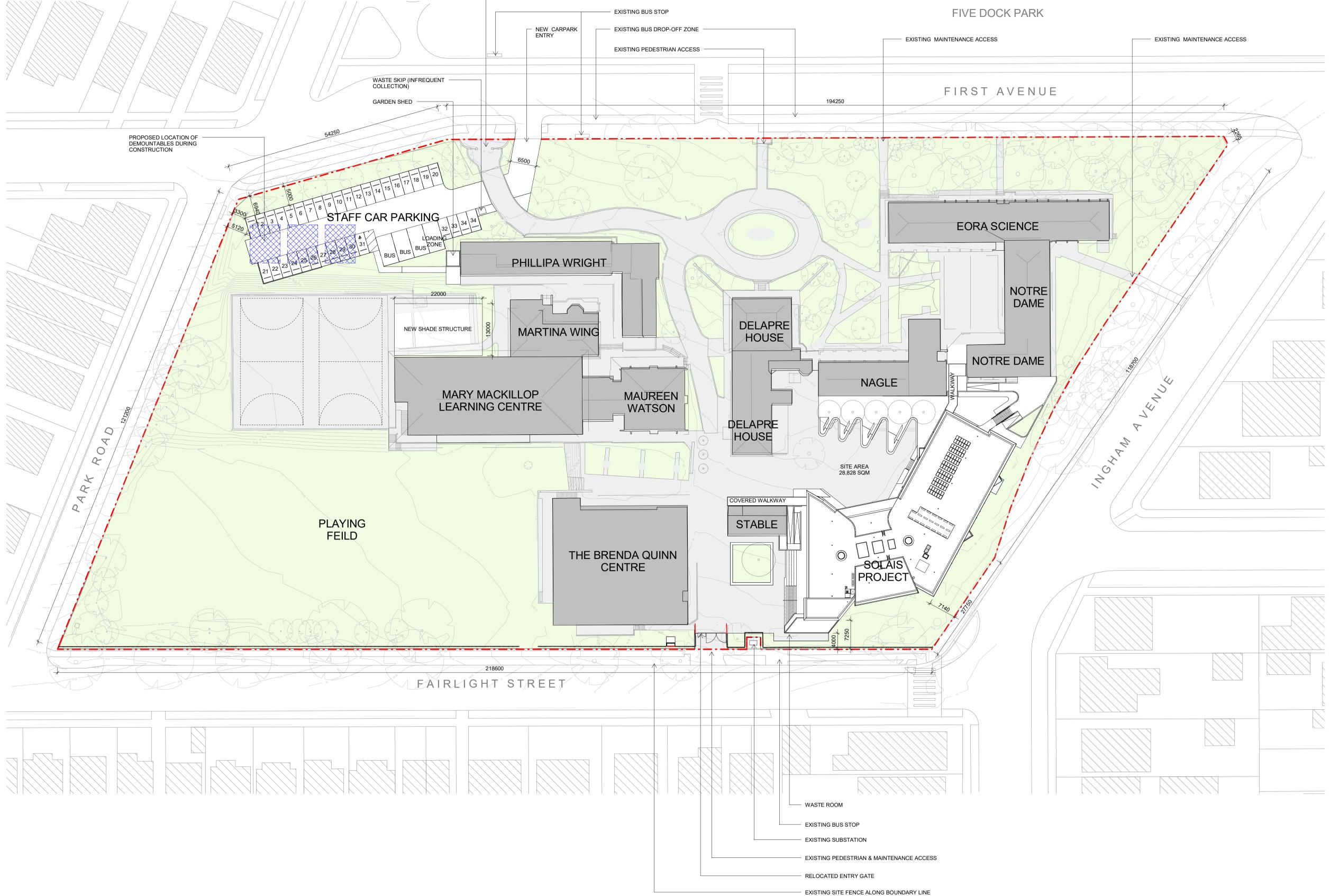






Attachment 3







FOR DEVELOPMENT APPLICATION

Builders/Contractors shall verify job dimensions before any job commences. Figured dimensions shall take precedence over scaled work. Work shall also conform to the specification, other drawings and job dimensions. All shop drawings shall be submitted to the Architect/Consultant and manufacture shall not commence prior to the return of inspected shop drawings signed by the Architect/Consultant. © Copyright 2008 All rights reserved

STATUS

PROPOSED SITE PLAN

DRAWING TITLE

121 First Avenue Five Dock, Sydney NSW

PROJECT ADDRESS

Sydney Catholic Schools

CLIENT TITLE

PROJECT TITLE

Domremy College Solais Project

ABN: 84006394261 NSW Nominated Architects:Tom Jordan 7521, Richard Leonard 7522, David Tordoff 8028

Melbourn/

A/135Ground FloorLevel 12,Sturt Street Southbank,11-17 Buckingham Street324 Queen Street,VIC 3006Surry Hills NSW 2010Brisbane Qld 4000T +61 3 9699 3644T +61 2 9660 9329T +61 7 3211 9821

Brisbane

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6	Amendment to Development Application	28.06.2018
5	Amendment to Development Application	02.05.2018
4	Issued for Development Application	02.03.2018
3	Issued for Development Application	16.02.2018
2	Issued for Development Application	25.01.2018
1	Consultant Coordination	18.01.2018
REV	DESCRIPTION	DATE



LEGEND

- - SITE BOUNDARY EXISTING BUILDINGS